Perpetual Pavements

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What is a Perpetual Pavement?

- 35+ Years of Service
- Minimal structural improvements
- No deep structural distresses
 - Only surface remedies needed

Perpetual Pavements in the U.S.



Goal of Perpetual Pavement Design

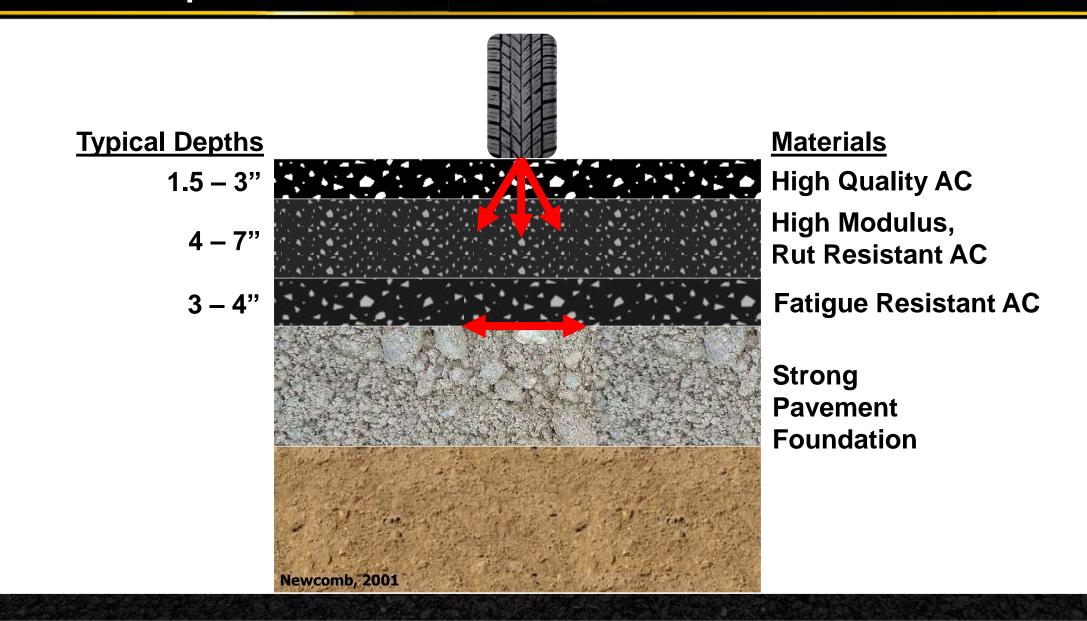
Design against deep structural distresses
 Bottom up fatigue cracking
 Structural Rutting



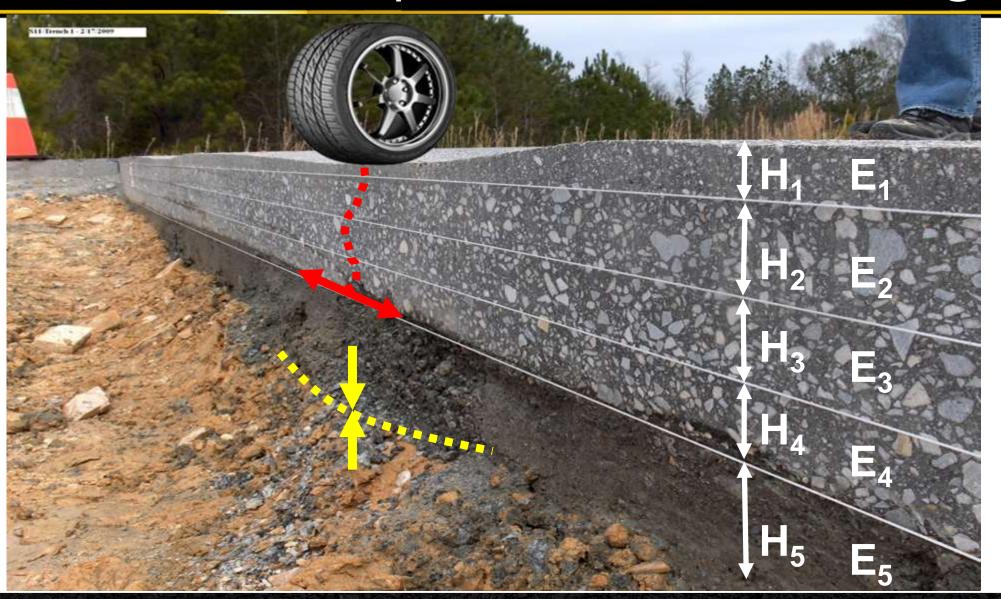


Results in a structure with Perpetual or Long-Life

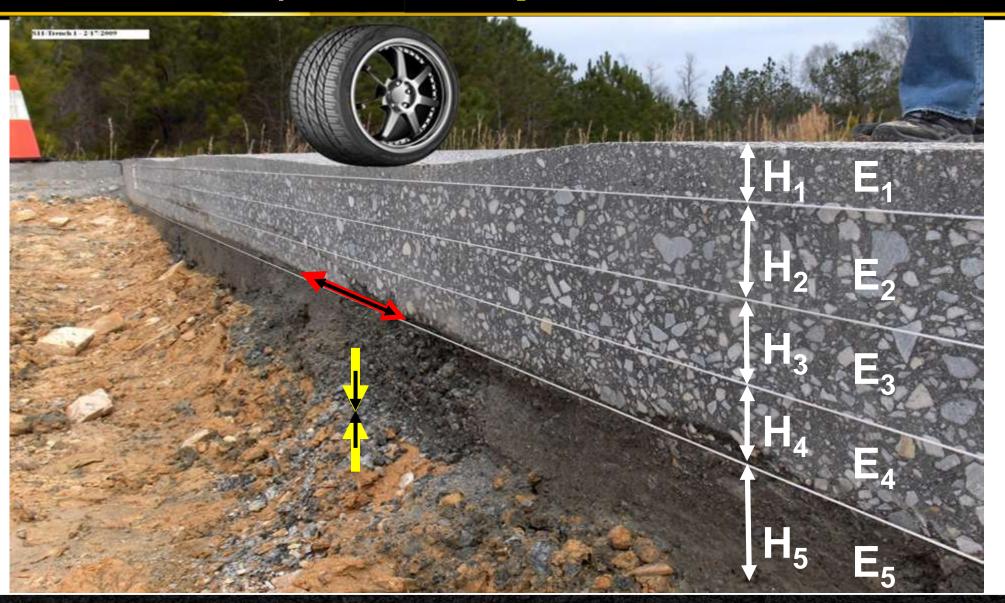
Perpetual Pavement Cross-Section



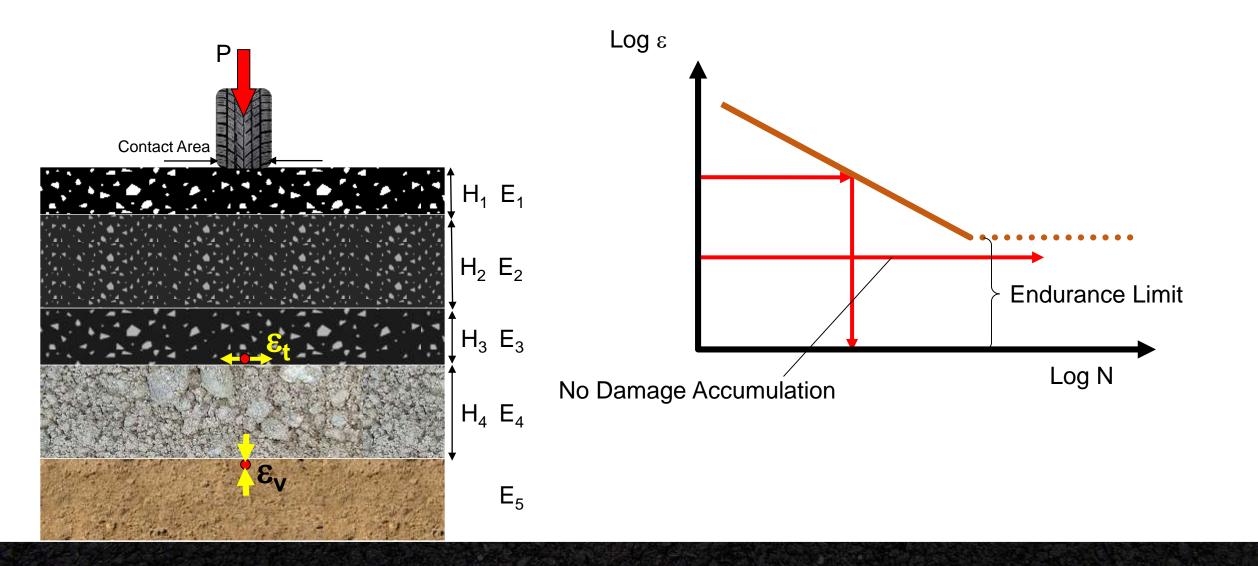
Mechanistic-Empirical Pavement Design



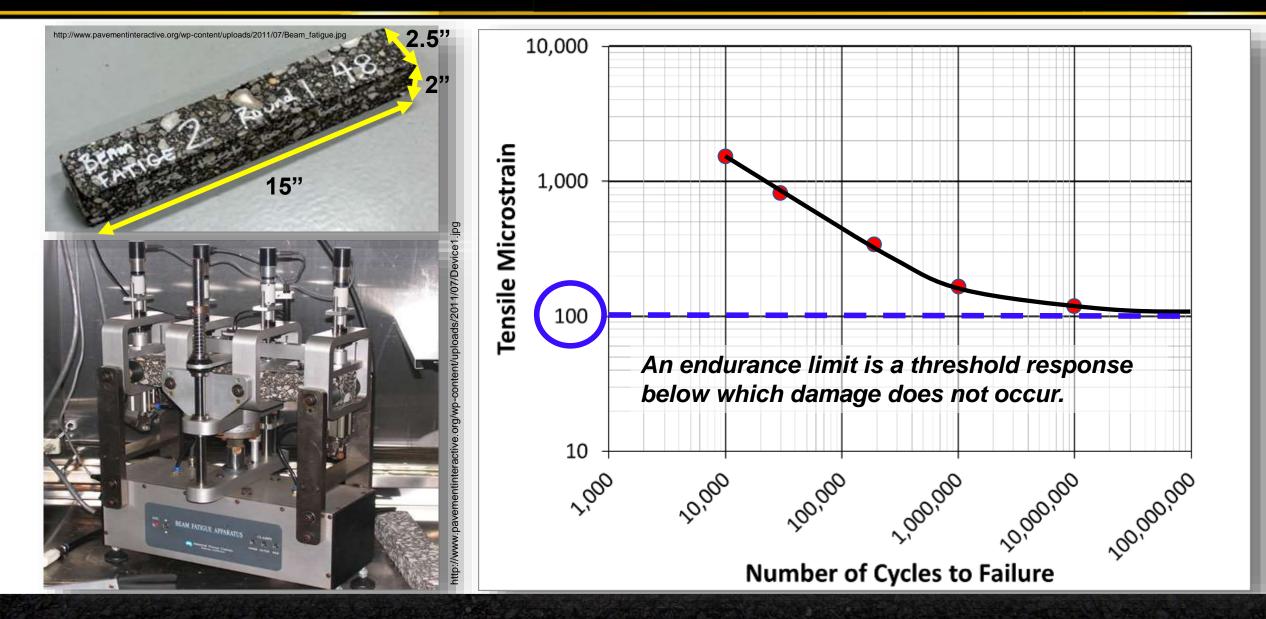
Mechanistic-Empirical Perpetual Pavement Design



Mechanistic-Empirical Perpetual Pavement Design



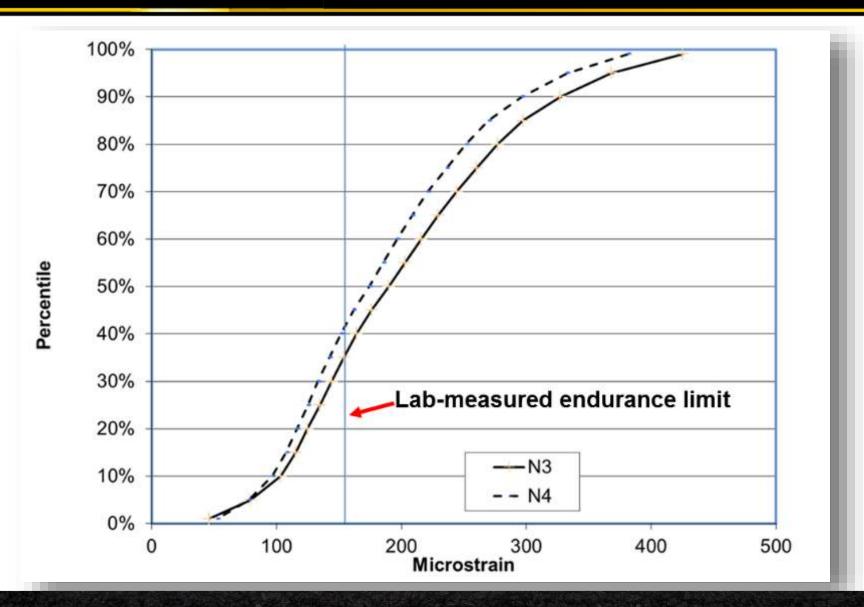
What is the **Endurance Limit** for AC?



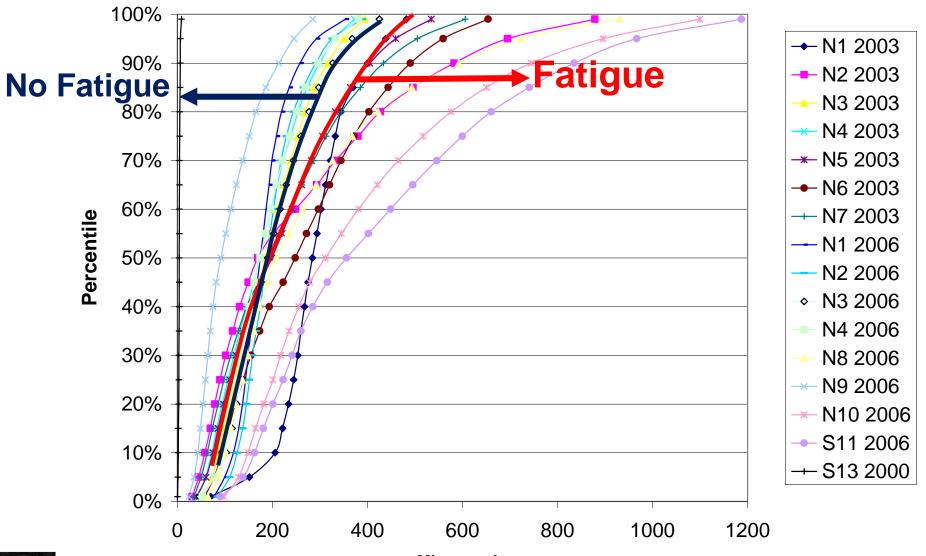
History of Endurance Limits

- 1972 Monismith estimates about 70 $\mu\epsilon$
- 2001 I-710 designed at 70 $\mu\epsilon$
- 2002 70 $\mu\epsilon$ used by APA
- 2007 NCHRP 9-38 Lab Study
 - + 100 $\mu\epsilon$ for unmodified binders
 - + 250 $\mu\epsilon$ for modified binders
 - Lab conditions more severe than field
- 2007 MEPDG uses 100 to 250 $\mu\epsilon$
- 2008 Measurements at NCAT Test Track show strains in perpetual pavements well exceeding laboratory values

Measured Horizontal Strains and Endurance Limits

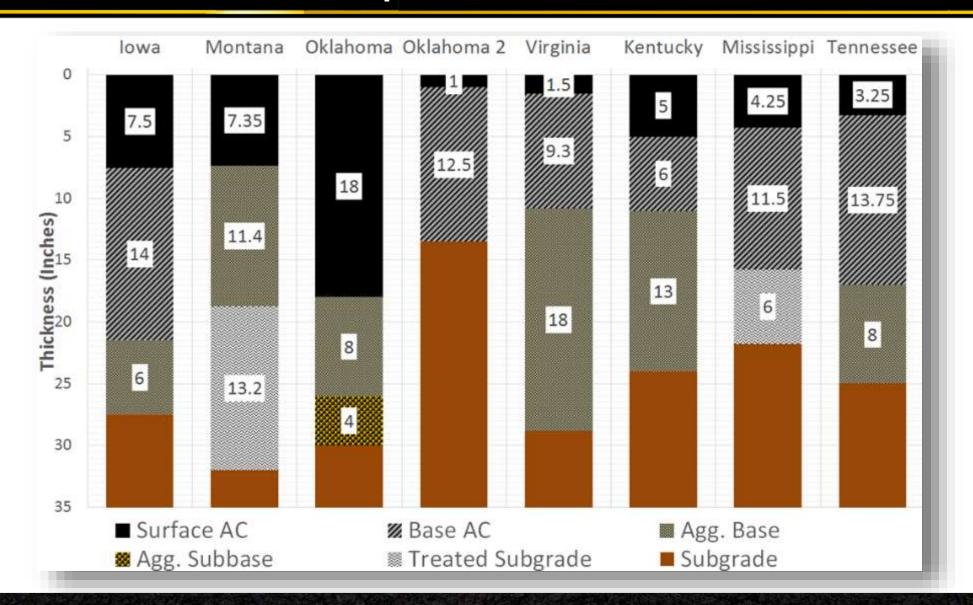


Horizontal Strain Distributions at NCAT Test Track



Microstrain

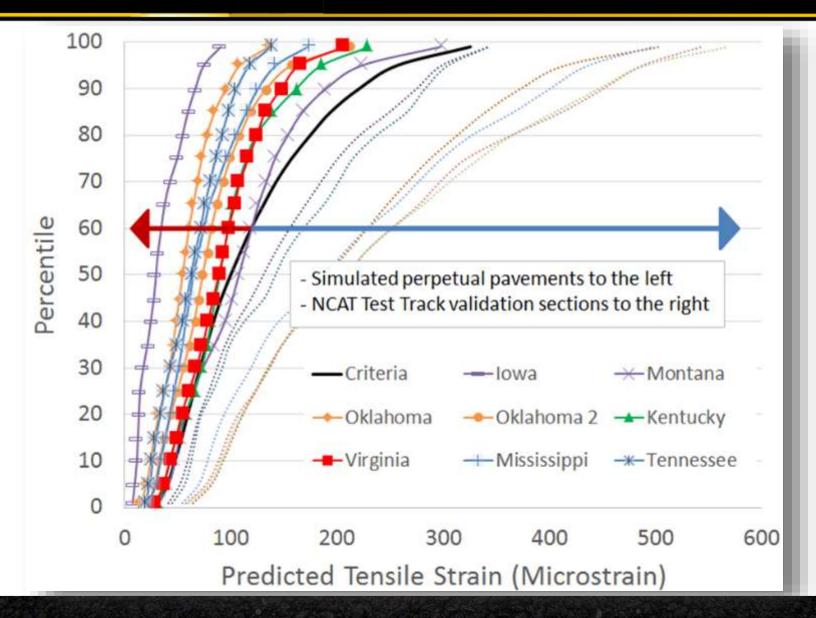
Evaluation of Perpetual Pavement Winners



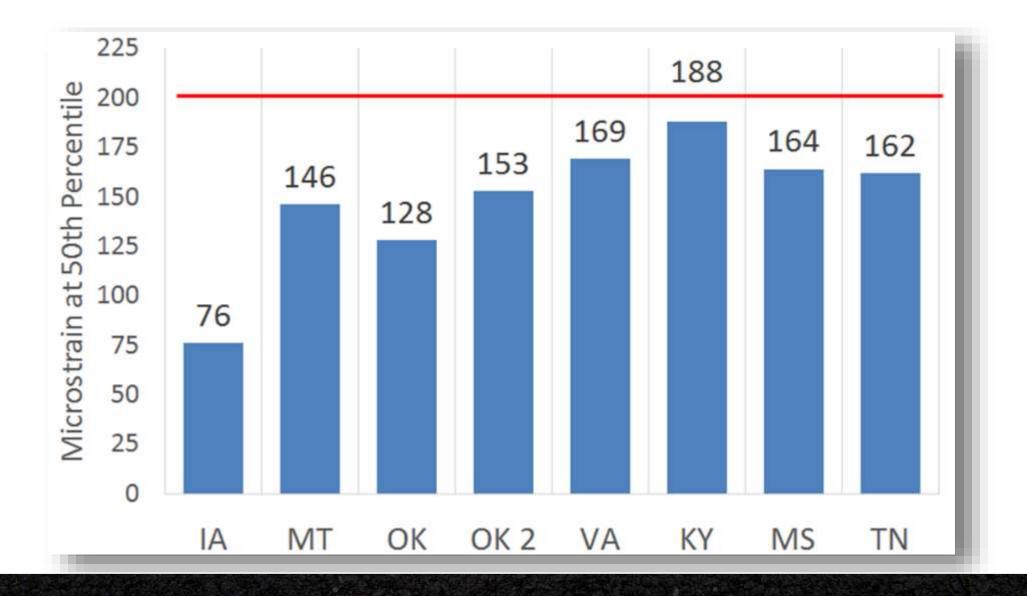
Award Winner Metrics

| State | Project | Year Honored | Service Years (Time of award) | Cumulative Traffic (Time of award) |
|-------------|-------------------------|-----------------|----------------------------------|---------------------------------------|
| lowa | I-80, MP 225.9 to 239.9 | 2002 | 38 | 32,000,000 ESAL |
| Montana | I-90 MP 439.33 to 445.4 | 2005 | 44 | 15,000,000 ESAL |
| Oklahoma | I-35, MP 185.6 to 192.6 | 2003 | 40 | 61,000,000 ESAL |
| Oklahoma | I-40, MP 160.2 to 165.5 | 2002 | 40 | 60,000,000 ESAL |
| Virginia | I-81, MP 318.4 to 324.9 | 2006 | 41 | 29,000,000 ESAL |
| Kentucky | I-65, Hart County | 2009 | 44 | 76,000,000 ESAL |
| Mississippi | I-22, Desoto County | 2007 | 39 | 60,000,000 ESAL |
| Tennessee | I-65, MP 22.4 to 32.56 | 2002 | 35 | 25,800,000 ESAL |

Horizontal Strain Distribution – Simulation Results



Award Winners – Vertical Strain Rutting Criteria



Need & Justification for Distribution-Based Design

- Pavements experience range of loading and environmental conditions
 - Results in wide range of strain responses
- Traditional M-E design uses transfer functions and sums damage vs. time
 - Fatigue transfer functions difficult to develop and may not be accurate
 - Transfer functions not needed with perpetual pavement design
- Designing with a strain distribution will limit fatigue cracking and avoid transfer functions
 - Also arrive at reasonable perpetual (maximum) pavement thicknesses
- Data from NCAT Test Track and validated with Perpetual Pavement Award Winners supports this approach
 - Horizontal tensile strain distribution for fatigue cracking
 - + 200 $\mu\epsilon$ compressive strain at the 50th percentile for rutting

Perpetual Pavement Design Tools



| PerRoadXPress | | |
|------------------------------------|---------------------|--|
| Press F1 to access full help file. | Press Shift+F1 to a | access context-senstive pop-up help. |
| Functional Classification: | Urban Collector | - |
| Two-Way AADT: | 1000 | (500 to 5000) |
| %Trucks: | 1 | (1 to 20) |
| %Growth: | 1 | (0 to 3) |
| Design Trucks: | 63482 | (Total Trucks in 30 Years) |
| Design ESALs: | 18917 | (Total ESALs in 30 Years) |
| AASHTO Soil Classification: | A-1-a ▼ | |
| Soil Modulus: | 29500 | (10,000 to 30,000 psi) |
| Aggregate Base Thickness: | 4 | (0 to 10 in.) |
| HMA Modulus: | 800000 | (400,000 to 1,000,000 psi) |
| | CALCULATE | |
| Calculated HMA | | in. |
| Design HMA | | in. Calculated thickness rounded up to nearest 0.25''. |
| | Exit H | lelp |

Key Features of PerRoad 4.4

- Layered elastic analysis
- Up to 5 pavement layers
- User enters design criteria
 - Strain distributions
 - Single strain values and control percentiles
 - Conventional M-E criteria with transfer functions

• Many built-in default parameters

- Material properties and variability
- Traffic and load distributions
- Program uses Monte Carlo simulation to simulate uncertainty in design

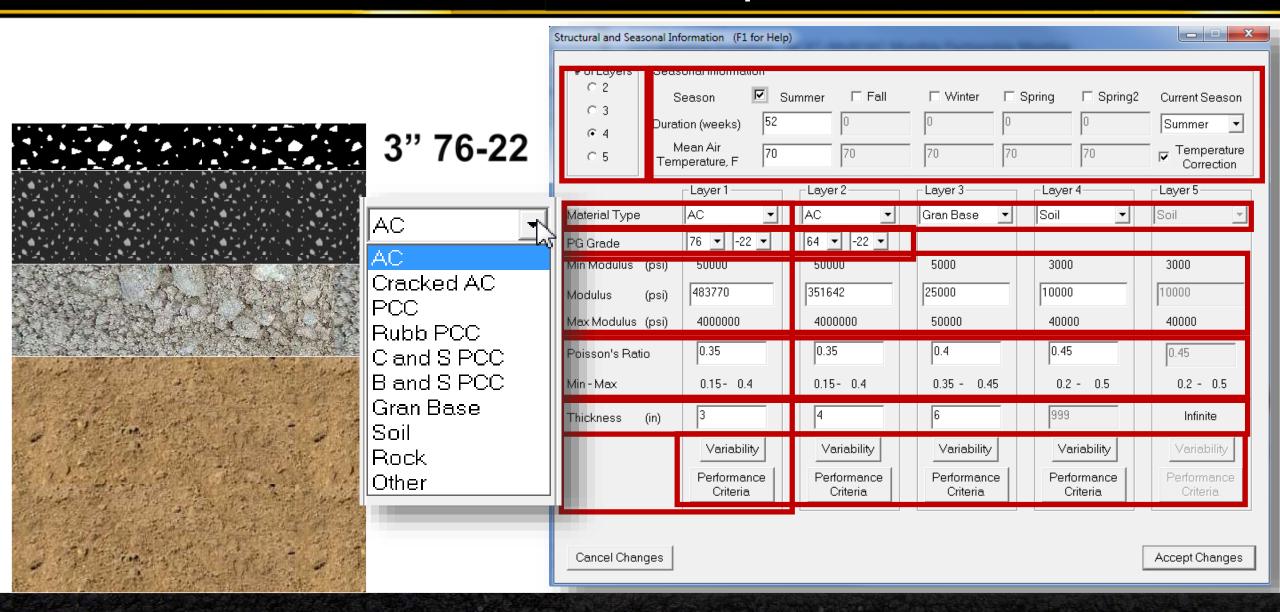
Design Example with PerRoad 4.4

- Interstate pavement
- 4 layer structure
 - 76-22 AC
 - 64-22 AC
 - Granular Base
 - Subgrade Soil
- Moderate Climate



http://www.flexiblepavements.org/sites/www.flexiblepavements.org/files/imagecache/awards_interior/awards/project_16-_interstate_271_kokosing.jpg

Structural Inputs



Input Variability

| put Variability | | | |
|------------------------------|----------------|-----------|---------------------------|
| Layer: AC | | | |
| _ Modulus Variability —— | | | |
| Distribution Type | Log-normal 💌 | and and | |
| Coefficient of Variation | 30 % | Frequency | |
| _ ⊤Thickness Variability— | | | [→] Modulus, psi |
| Distribution Type | Normal 💌 | | |
| Coefficient of Variation | 5 % | Frequency | |
| | | E | |
| Cancel Changes | Accept Changes | | Thickness, in |

Performance Criteria – Fatigue Cracking

| ayer Performance Criteria (Press F1 | for Help) | C. Street William | the Property of | Summer Summer | × |
|-------------------------------------|---------------|-------------------|-----------------------|-----------------|---------------|
| Layer: 2 | | | Note: The transfer fu | nctions are for | strain only. |
| Position Criteria | Threshold | Target Percentile | Transfer Function | k1 | k2 |
| Г Тор | | | | | |
| IT Middle | | | | | |
| IT Bottom | | | | | |
| | | | | | |
| Note: The following sign conve | ation is used | | | | |
| Negative = Tension | | | | | |
| Positive = Compression | | | | | |
| Deflection is Positive Downwar | d | | | | |
| | | | | 41 | |
| Cancel Changes | | | | A | ccept Changes |
| | | | | | |

Performance Criteria – Fatigue Cracking

| Layer Performance Criteria (Press F1 for Help) | P. Long. M. Str. | Street, Miles | a range or | and later. | × |
|---|------------------|-------------------|--------------------------|--------------------|-----------|
| Layer: 2 | | | Note: The transfer funct | ions are for strai | n only. |
| Position Criteria | Threshold | Target Percentile | Transfer Function | k1 | k2 |
| Г Тор | | | | | |
| ☐ Middle | | | | | |
| ✓ Bottom ✓ Horizontal Stress Vertical Stress Vertical Stress Principal Stress Horizontal Strain Vertical Strain Principal Strain Negative = Vertical Deflection Horizontal Strain Distribution Positive = Compression Deflection is Positive Downward | 0 | 50 | | | |
| Cancel Changes | | | | Accep | t Changes |

Performance Criteria – Fatigue Cracking

| Layer Performance Criteria (Press F1 for Help) | P. Const. J. Mar. | From High | and the second second | Summer Summer | × |
|---|---------------------------|-------------------|------------------------|-------------------|-------------|
| Layer: 2 | | | Note: The transfer fur | nctions are for s | train only. |
| Position Criteria | Threshold | Target Percentile | Transfer Function | k1 | k2 |
| Г Тор | | | | | |
| □ Middle | | | | | |
| I ■ Bottom Horizontal Strain Distribution | Percentile Microstrain | | | | |
| | 95th -257 | | | | |
| | 85th -194 | | | | |
| Note: The following sign convetion is used | 75th -158 | | | | |
| Negative = Tension | 65th -131 | | | | |
| Positive = Compression Deflection is Positive Downward | 55th -110 | | | | |
| | Load Default Distribution | | | | |
| Cancel Changes | Enter Endurance Limit | | | Acc | ept Changes |

Performance Criteria – Rutting

| ayer Performance Criteria (Press F1 for Help) | R. Same | 7.58 | Come The | ng 7 Spring | Summer Summer | × |
|---|-----------|-------------|-------------------|-----------------------|-----------------|--------------|
| Layer: 4 | | | | Note: The transfer fu | nctions are for | strain only |
| Position Criteria | Threshold | | Target Percentile | Transfer Function | k1 | k2 |
| | | | | | | |
| ✓ Top Vertical Strain | 200 | microstrain | 50 | Γ | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| Note: The following sign convetion is used | | | | | | |
| Negative = Tension | | | | | | |
| Positive = Compression Deflection is Positive Downward | | | | | | |
| Deflection is Positive Downward | | | | | | |
| | | | | | | |
| Cancel Changes | | | | | Ac | cept Changes |
| | | | | | | |
| | | | | | | |

Traffic Inputs

| oading Conditions | (F1 for Help) | | | | • | 1.00 | | | |
|---------------------------------------|-----------------|-------------------------------|---------------------|-------------------|---------|-------------------------------|---------|-------------------|-----------------------------------|
| General Traffi Two-W Axles Grou | 'ay AADT 👖 | 1000 | % Tri % Truck Gr | ucks 10 owth 4 | _ | cks in Desig actional Dist | | | ut Load Spectra y Vehicle Type |
| | · · · / | | | | | scuonai Dist | | | |
| Loading Confi | | eck All That. | | | | | | Cur | rrent Configuration |
| 00-00 50 | Single .43 % | <mark>00-00</mark> | ▼ Tandem 48.81 % | <mark>10=</mark> | 0.76 | "m "% | 0 | - 195 | ingle 🔻 |
| Current Axle L | .oad Distributi | ion | | | | | | | |
| Axle Wt kip | % Axles | Axle Wt kip | % Axles | Axle Wt kip | % Axles | Axle Wt kip | % Axles | Axle Wt kip | % Axles |
| | 0 | | 0.35 | 48-50 | 0 | 72-74 | 0 | 96-98 | 0 |
| 2-4 | 4.46 | 26-28 | 0.2 | 50-52 | 0 | 74-76 | 0 | 98-100 | 0 |
| 4-6 | 9.13 | 28-30 | 0.1 | 52-54 | 0 | 76-78 | 0 | 100-102 | 0 |
| 6-8 | 11.32 | 30-32 | 0.05 | 54-56 | 0 | 78-80 | 0 | 102-104 | 0 |
| 8-10 | 19.55 | 32-34 | 0.04 | 56-58 | 0 | 80-82 | 0 | 104-106 | 0 |
| 10-12 | 25.5 | 34-36 | 0.02 | 58-60 | 0 | 82-84 | 0 | 106-108 | 0 |
| 12-14 | 14.57 | 36-38 | 0.01 | 60-62 | 0 | 84-86 | 0 | 108-110 | 0 |
| 14-16 | 6.42 | 38-40 | 0.01 | 62-64 | 0 | 86-88 | 0 | 110+ | 0 |
| 16-18 | 3.84 | 40-42 | 0 | 64-66 | 0 | 88-90 | 0 | _ | 100 |
| 18-20 | 2.39 | 42-44 | 0 | 66-68 | 0 | 90-92 | 0 | Total | 100 |
| 20-22 | 1.37 | 44-46 | 0 | 68-70 | 0 | 92-94 | 0 | | |
| 22-24 | 0.68 | 46-48 | 0 | 70-72 | 0 | 94-96 | 0 | | |
| Cancel Chang | les | | Import | :Load Spe | ctra S | ave Load Sp | pectra | | Accept Changes |

Vehicle Type Distribution

| /ehicle Type Distribution (Press F1 for | Help) | _ | | | X |
|---|-----------------|--------------------|--|--------------------|----------------|
| F | Roadway Functio | nal Classification | Rural Interstate | | -2 |
| | Vehicle | | and the second | Number of Axles Pe | er Vehicle |
| | Classification | % AADTT | Single | Tandem | Tridem |
| | 4 | 1.2 | 1.62 | 0.39 | 0 |
| ą | 5 | 9.4 | 2 | 0 | 0 |
| 商 | 6 | 3.3 | 1.02 | 0.99 | 0 |
| - ee | 7 | 0.5 | 1 | 0.26 | 0.83 |
| | 8 | 7.4 | 2.38 | 0.67 | 0 |
| 32 | 9 | 68.9 | 1.13 | 1.93 | 0 |
| | 1.1.1 | 1.2 | 1.19 | 1.09 | 0.89 |
| | 1 1 | 6.1 | 4.29 | 0.26 | 0.06 |
| | 12 | 0.8 | 3.52 | 1.14 | 0.06 |
| | 13 | 1.2 | 2.15 | 2.13 | 0.35 |
| | Total | 100 | | | |
| Cancel Changes | | | | | Accept Changes |

Axle Types & Load Spectra

| oading Conditions | (F1 for Help) | | | | ۰. | 1.1 | | · · · · | |
|---------------------------------------|----------------------------------|--------------------------|--------------------------|-------------------|---------|-------------------------------|------------------------|-------------------|------------------------------------|
| – General Traff Two-W Axles Gro | /ay AADT | 1000 136 | % Tru % Truck Gro | icks 10 owth 4 | _ | cks in Desig ectional Dist | | % Inp % b | out Load Spectra y Vehicle Type |
| | igurations (C Single .43 % | heck All That | Apply) Tandem 48.81 % | ()) = | Tride | ۳m % | <mark>0—0</mark> □ st | eer 📕 💻 | rrent Configuration ingle |
| Axle Wt kip | % Axles | ien Axle Wt kip | % Axles | Axle Wt kip | % Axles | Axle Wt kip | % Axles | Axle Wt kip | % Axles |
| · · · · | 0 | 24-26 | 0.35 | 48-50 | 0 | 72-74 | 0 | 96-98 | 0 |
| 2-4 | 4.46 | 26-28 | 0.2 | 50-52 | 0 | 74-76 | 0 | 98-100 | 0 |
| 4-6 | 9.13 | 28-30 | 0.1 | 52-54 | 0 | 76-78 | 0 | 100-102 | 0 |
| 6-8 | 11.32 | 30-32 | 0.05 | 54-56 | 0 | 78-80 | 0 | 102-104 | 0 |
| 8-10 | 19.55 | 32-34 | 0.04 | 56-58 | 0 | 80-82 | 0 | 104-106 | 0 |
| 10-12 | 25.5 | 34-36 | 0.02 | 58-60 | 0 | 82-84 | 0 | 106-108 | 0 |
| 12-14 | 14.57 | 36-38 | 0.01 | 60-62 | 0 | 84-86 | 0 | 108-110 | 0 |
| 14-16 | 6.42 | 38-40 | 0.01 | 62-64 | 0 | 86-88 | 0 | 110+ | 0 |
| 16-18 | 3.84 | 40-42 | 0 | 64-66 | 0 | 88-90 | 0 | | |
| 18-20 | 2.39 | 42-44 | 0 | 66-68 | 0 | 90-92 | 0 | Total | 100 |
| 20-22 | 1.37 | 44-46 | 0 | 68-70 | 0 | 92-94 | 0 | | |
| 22-24 | 0.68 | 46-48 | 0 | 70-72 | 0 | 94-96 | 0 | | |
| Cancel Chang | jes | | Import | Load Spe | ctra S | ave Load S | pectra | | Accept Changes |

PerRoad Thickness Design Module

| | - Thickness | Pavement Layers: 4 Layer 1 AC | Layer 2 AC 4 6 | Layer 4 Soil | Layer 5 Soil Infinite | Reliability Analysis Set Monte Carlo Cycles Perform Analysis | |
|--|------------------|-------------------------------------|---|-----------------|-----------------------------|--|----|
| 🙎 Save As | Perpetual F | Pavement Design Results | : Conventional Design with Transf | er Functions — | | Monte Carlo Cycles | |
| Save in: Desktop Name Calibraries David Timm | ▼ Size | 🗢 🛍 📸 📰 ▾ Item type | Date modified | | Ē | Number of Monte Carlo Cycles | |
| Computer Network Adobe CS6 Design Standard AFD60 2017 | | File folder File folder | 8/27/2014 4:32 PM 1/10/2017 11:08 AM | | - | Cancel | ОК |
| File name: Trial 1 kls | 6 | | | | Save | | |
| Save as type: PerRoad Raw Data (*xls | Disclaime | er | Cost Analys | is Export | Formatted Data to EXCE | Leave Module | |

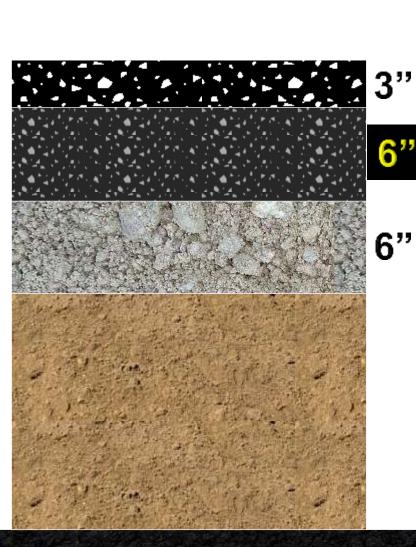
Simulation Results

| Layer | Location | Criteria | Units | Target Value | Target Percentile | Actual Percentile | Pass/Fail? |
|-------|----------|-----------------|-------|--------------|-------------------|-------------------|------------|
| 2 | Bottom | Tensile Strain | micr | -257. | 95 | 96.2 | Pass |
| | | | | -194. | 85 | 85.4 | Pass |
| | | | | -158. | 75 | 68. | Fail |
| | | | | -131. | 65 | 53.4 | Fail |
| | | | | -110 | 55 | 41 | Fail |
| 4 | Тор | Vertical Strain | micr | 200. | 50. | 31.6 | Fail |

• Pavement is NOT perpetual

- Failing in both bottom-up fatigue and rutting
- Change design thicknesses and analyze again

2nd Design Iteration



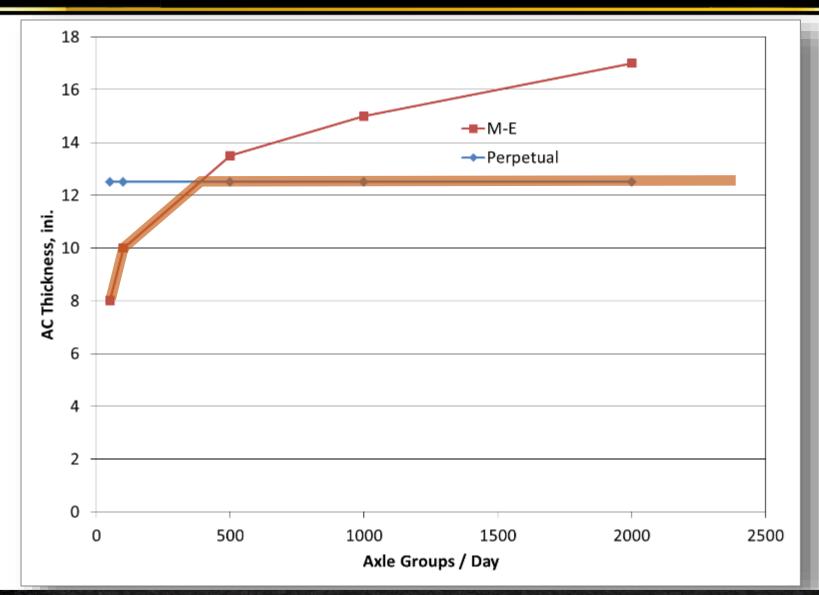
| t & Desi | gn Module (F | 1 for Help) | | | | | | | | | | | | |
|------------------|---------------|-----------------------------------|--------------------|---|--------------------------|-------|-----------------------------------|--------|-----------------------------|--|----------|--|------|-------------|
| | P | ayer1 AC | Layer 2 AC 6 | | Layer 3 Gran Bas 6 | e | Layer 4 Soil 999 | | _ayer 5 Soil Infinite | Reliabi | lity An | alysis Set Monte Carlo Perform Anal | - | |
| erpetua Layer | | Design Results: (Criteria | Conventio | | | | nctions Below Critical | | Damage/Mill | ion Axle | <u> </u> | ′ears to D=0.1 | Year | s to D=1.0 |
| rpetua | I Pa∨ement | Design Results: F | Percentile | Respon | ses | | III | | | | | | | 4 |
| .ayer | Location | Criteria | Units | Target | Value | | Target Pe | rcenti | | Actual Perce | entil | Pass/Fail? | | |
| 1 | Bottom Top | Tensile Strain Vertical Strain | micr | -257. -194. -158. -131. -110. 200. | | | 95 85 75 65 55 50. | | | 39.6 36. 31.6 32. 59.8 55.2 | | Pass Pass Pass Pass Pass Pass | | |
|)isclain | ner | | | | Cost Ana | lysis | Export For | matte | ed Data to EXC | EL | | | l | .eave Modul |

Additional Design Examples

| Subgrade | Base | Ca | Range of | | | | |
|----------|----------|-------------|------------|------------|---------|-------------------|--|
| Mr (ksi) | Mr (ksi) | Minneapolis | Phoenix | Baltimore | Average | Maximum | |
| | 3 | (PG 64-34) | (PG 70-22) | (PG 64-22) | • | Thicknesses (in.) | |
| 5 | 30 | 12.5 | 15.5 | 14 | 14.0 | 12.5-15.5 | |
| 5 | 50 | 12 | 15 | 14 | 13.7 | 12-15 | |
| 5 | 100 | 12 | 14 | 13.5 | 13.2 | 12-14 | |
| 10 | 30 | 10.5 | 14 | 12 | 12.2 | 10.5-14 | |
| 10 | 50 | 10.5 | 13 | 12 | 11.8 | 10.5-13 | |
| 10 | 100 | 10 | 12 | 11 | 11.0 | 10-12 | |
| 20 | 30 | 9 | 12.5 | 10 | 10.5 | 9-12.5 | |
| 20 | 50 | 8.5 | 12.5 | 9.5 | 10.2 | 8.5-12.5 | |
| 20 | 100 | 8 | 12 | 9 | 9.7 | 8-12 | |

Design Comparison – Perpetual vs M-E

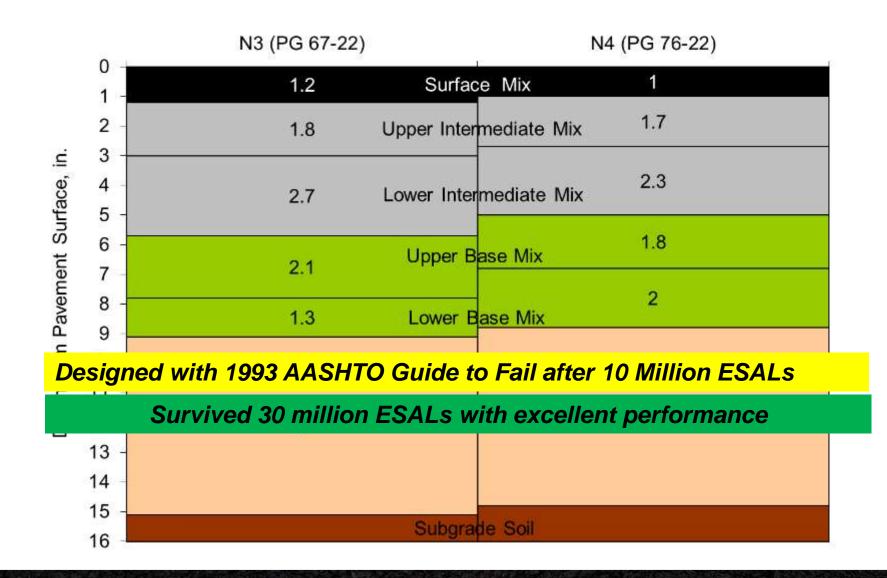
- Minneapolis
- 6" Aggregate Base
 - 30 ksi
- 5 ksi soil
- M-E 35 year analysis



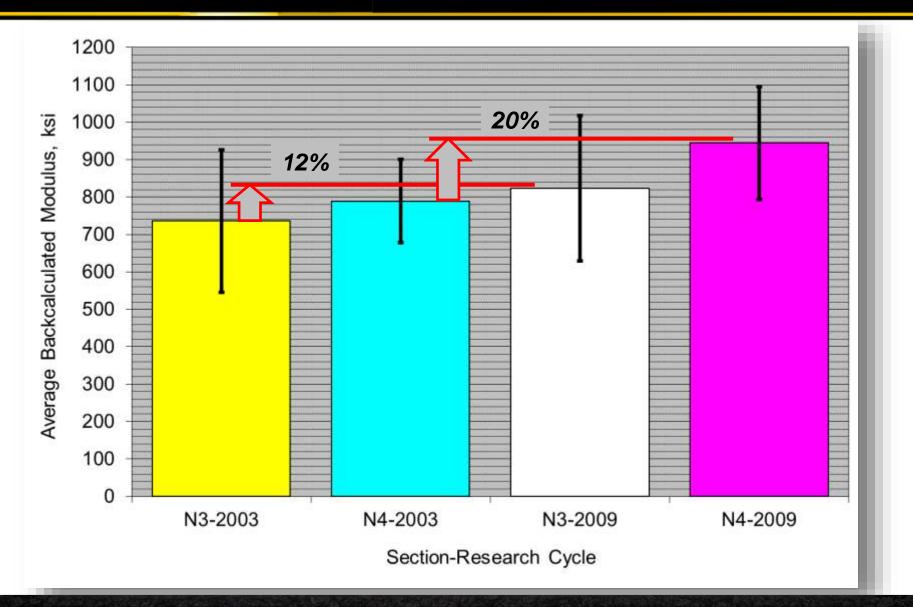
NCAT Test Track – Perpetual Experiments



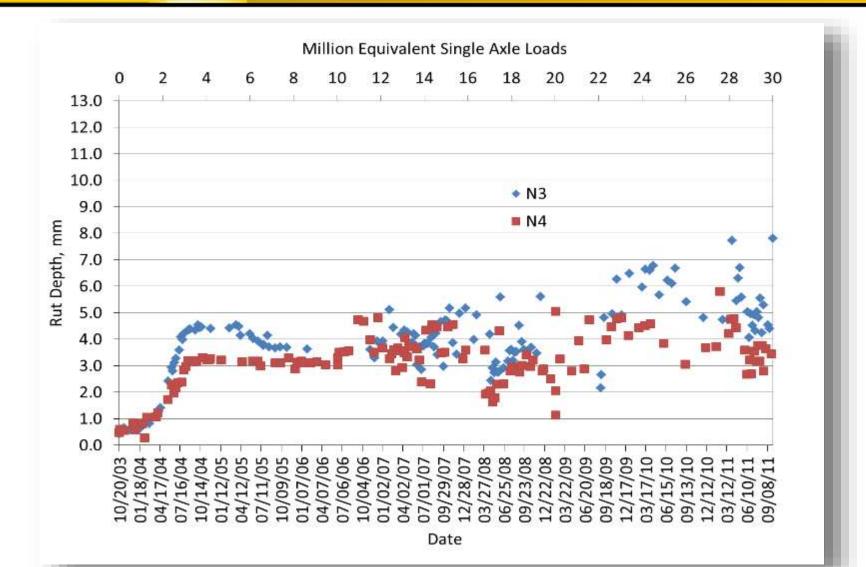
Test Sections – Experiment 1



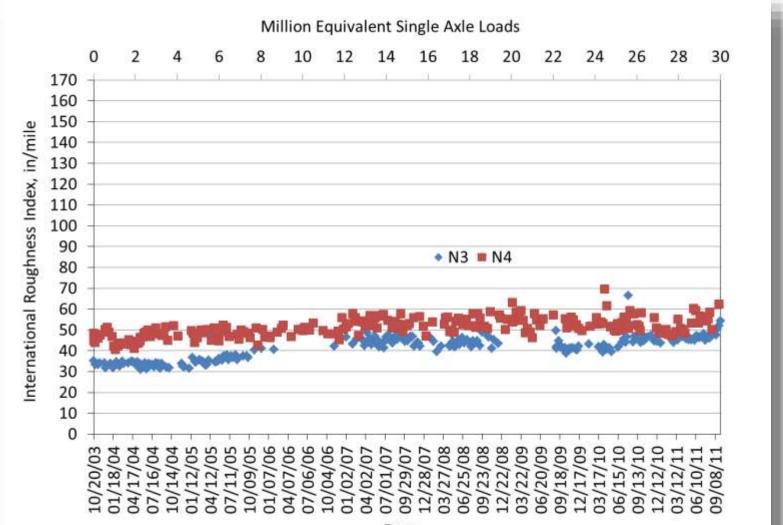
In-Place Modulus vs Time



Rutting Performance

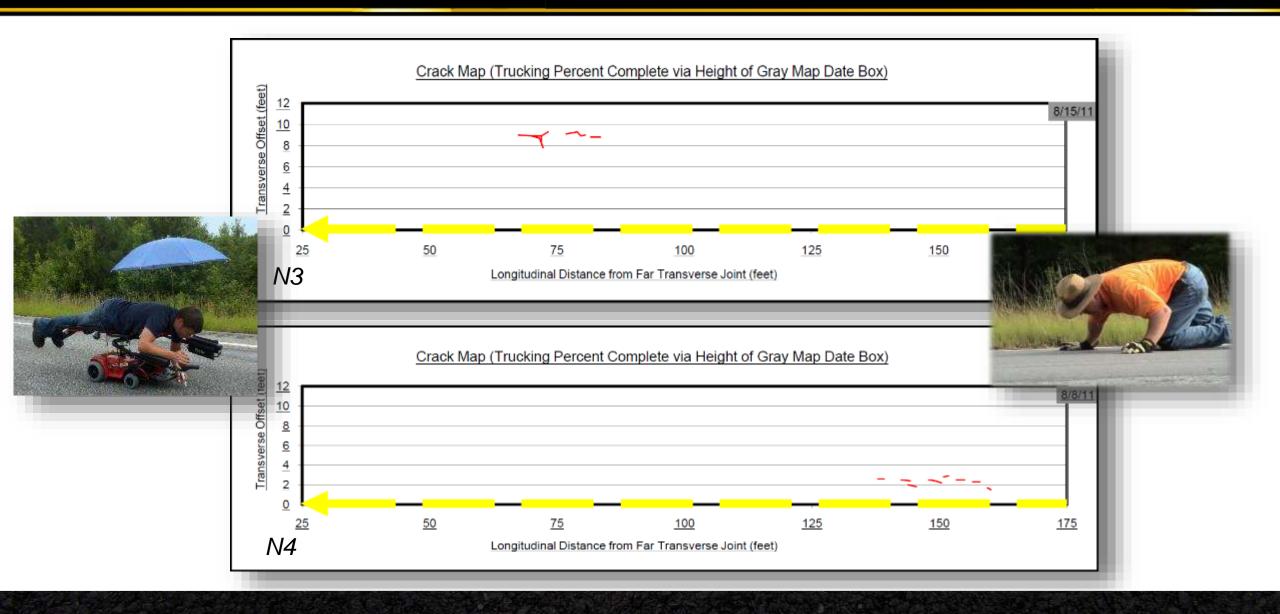


Ride Quality



Date

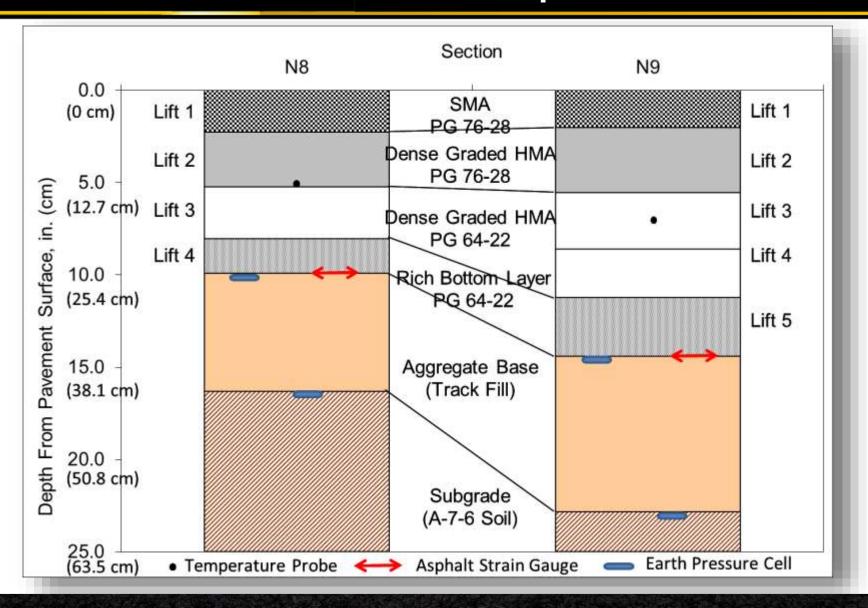
Cracking Performance



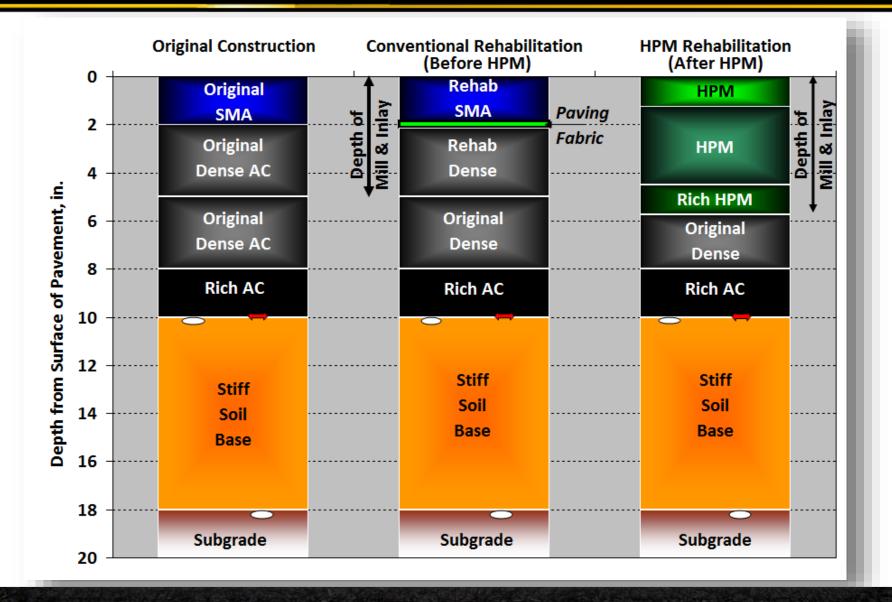
Forensic Trenching



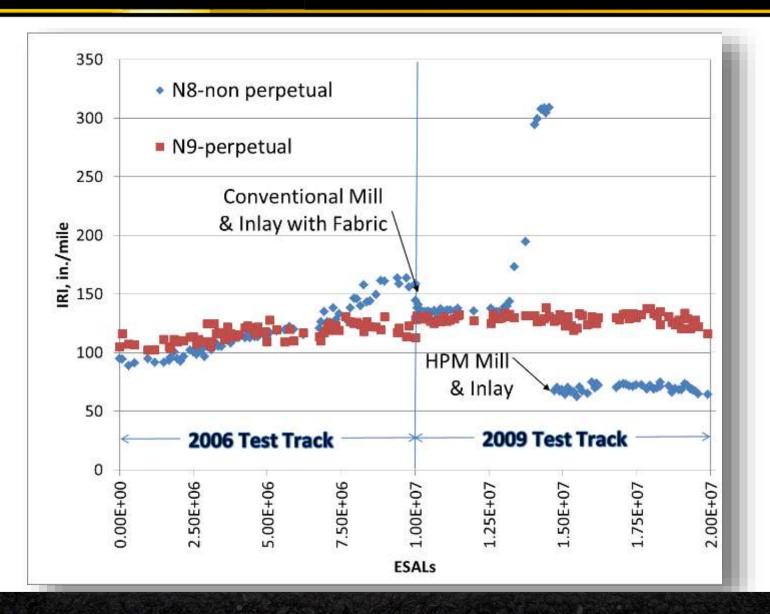
Test Sections – Experiment 2



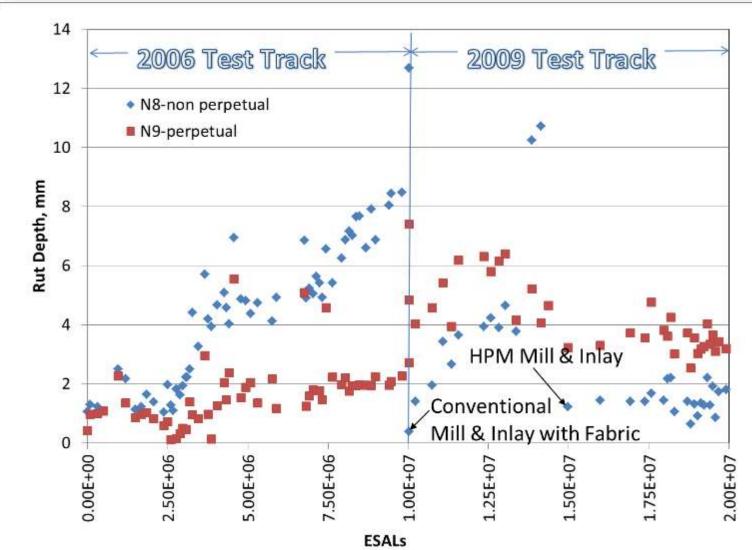
N8 Rehabilitation



Section Performance - IRI



Section Performance - Rutting

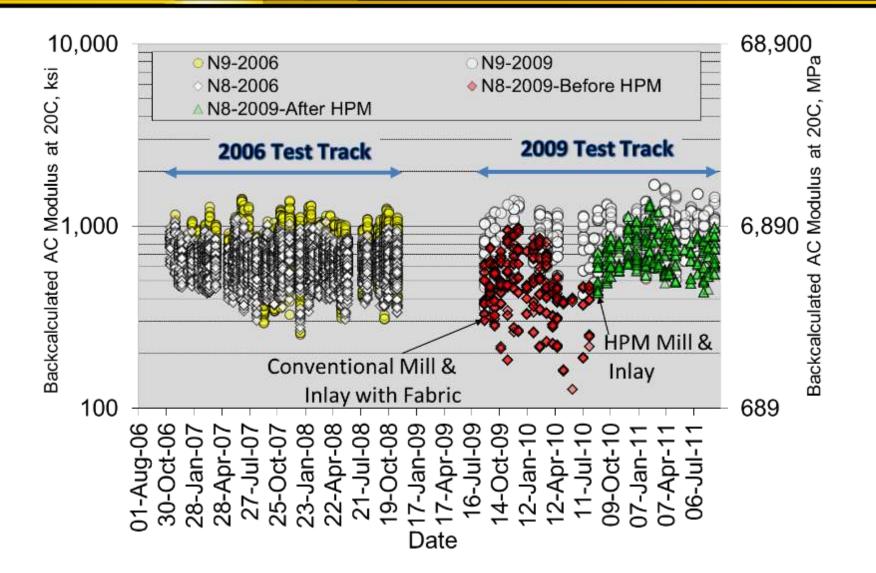


JALS

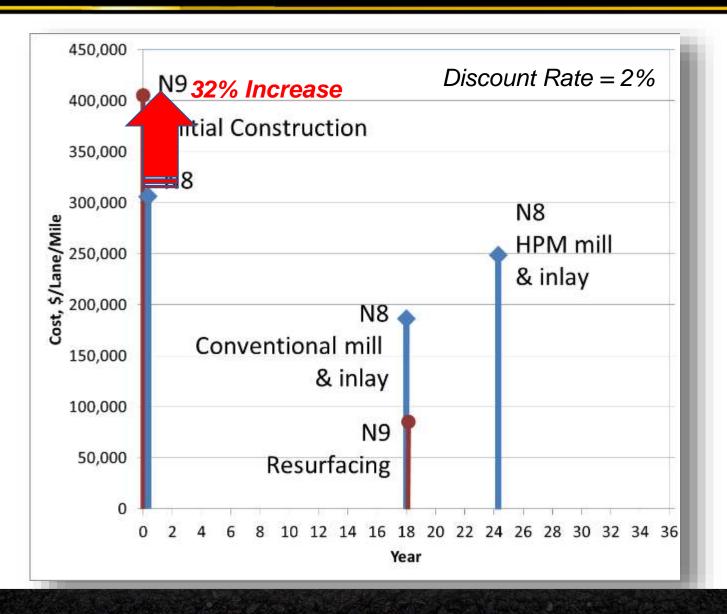
N8 After 1st Rehabilitation @ 3.5 MESAL



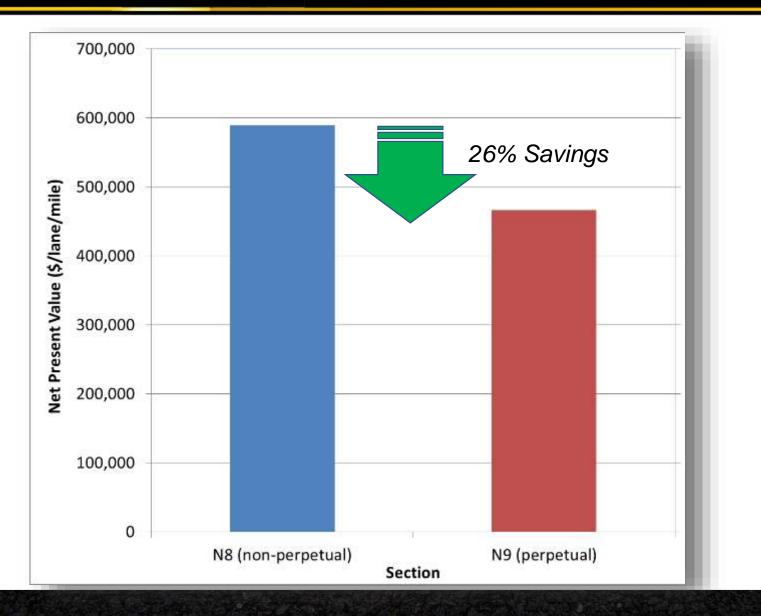
AC Modulus vs Date



Life Cycle Cost Analysis – Cash Flow Diagram



Life Cycle Cost Analysis – Net Present Value



Summary & Conclusions

- Perpetual pavements widely recognized across the U.S.
- Perpetual pavements don't have deep structural problems
 - Surface remedies make them an attractive option
- Perpetual pavements can be designed using mechanistic principles
 - Strain distributions developed at NCAT Test Track and validated with award winners
- PerRoad incorporates strain distribution design & Monte Carlo simulation to produce reasonable perpetual pavement cross-sections
 - Can be used to find maximum thicknesses
- Case studies from Test Track highlight key features of perpetual pavement
 - Tend to gain modulus over time
 - Exhibit excellent performance
 - Stable ride quality
 - Minimal rutting
 - No deep structural distresses
 - Cost effective

Thank you!

