



# **Percent within Limits (PWL) and Balanced Mix Design (BMD):**

**An Update on WisDOT's Current Practice and Future Plans**

**WAPA Annual Conference**

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**PWL:**

**An Update on WisDOT's Current Practice and Future Plans**

**Dan Kopacz, PE**

# PWL Updates

- History of PWL
- 2022 PWL summary data
- Where are we headed?



# Quality Assurance Goals

- Remain FHWA Compliant
  - Code of Federal Regulations (CFR)
- Verify Contractor Data
  - F&t is used to verify contractor data
- Increase Consistency Near the Target
  - Percent Within Limits (PWL)
- Ensure Adequate Performance
  - Set appropriate specification limits



# Where we were





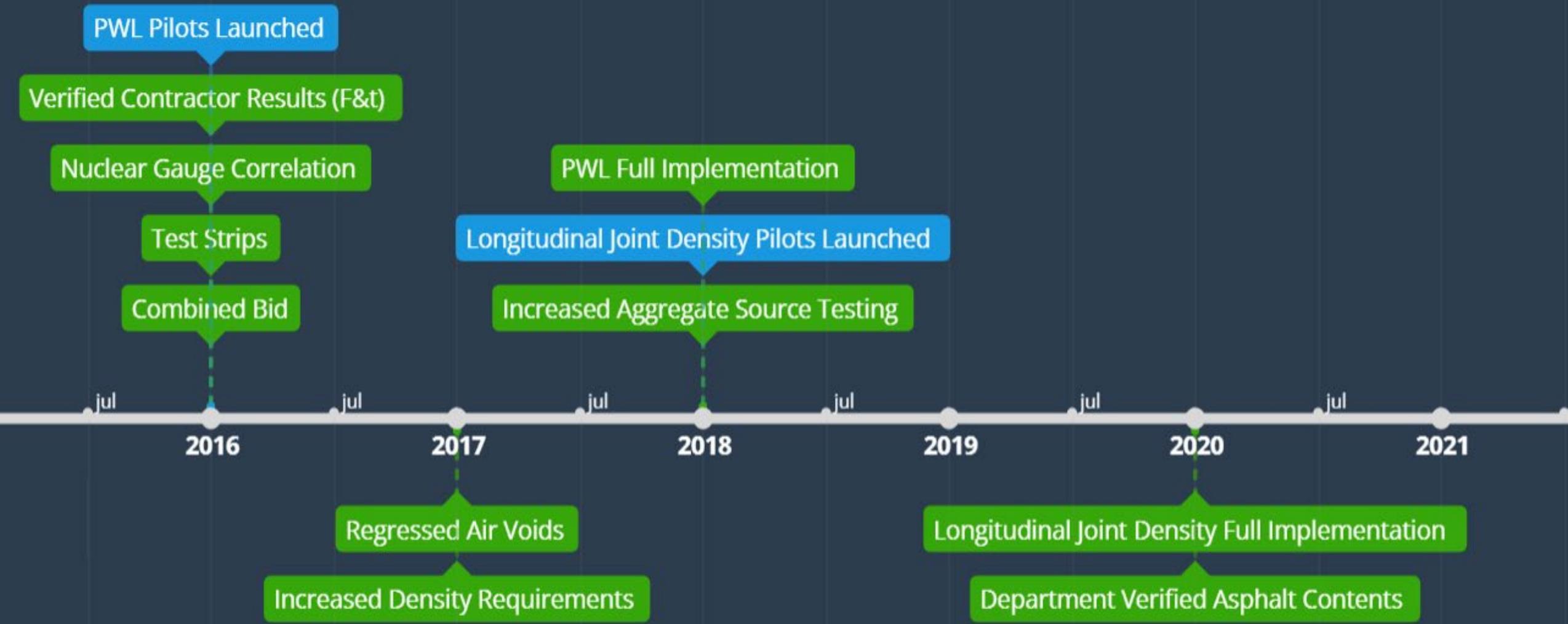
FHWA Review

VMA increases for 9.5mm and 12.5mm mixes.

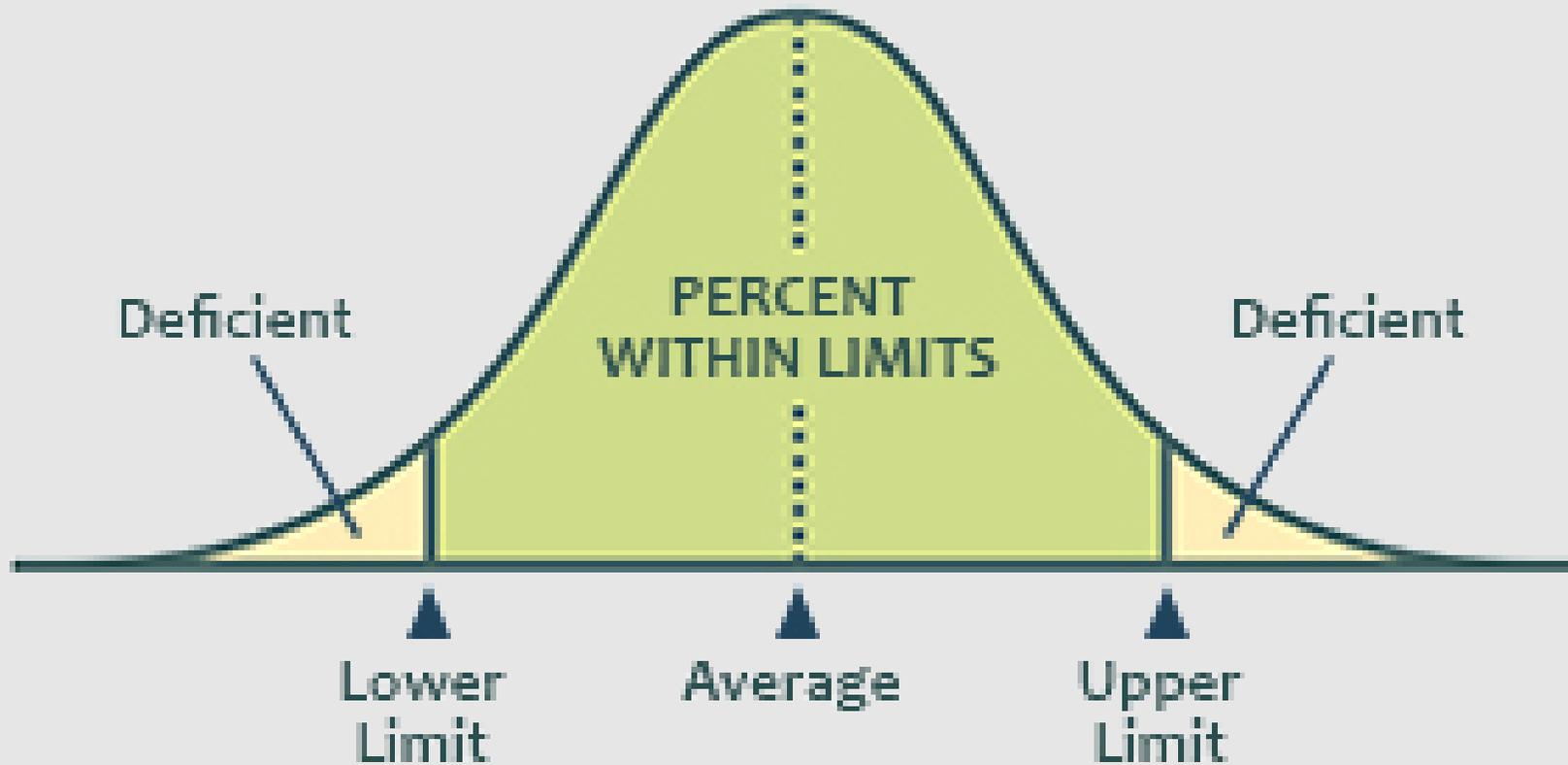
Increased Testing Frequencies

Binder Temperature Guidance Updated

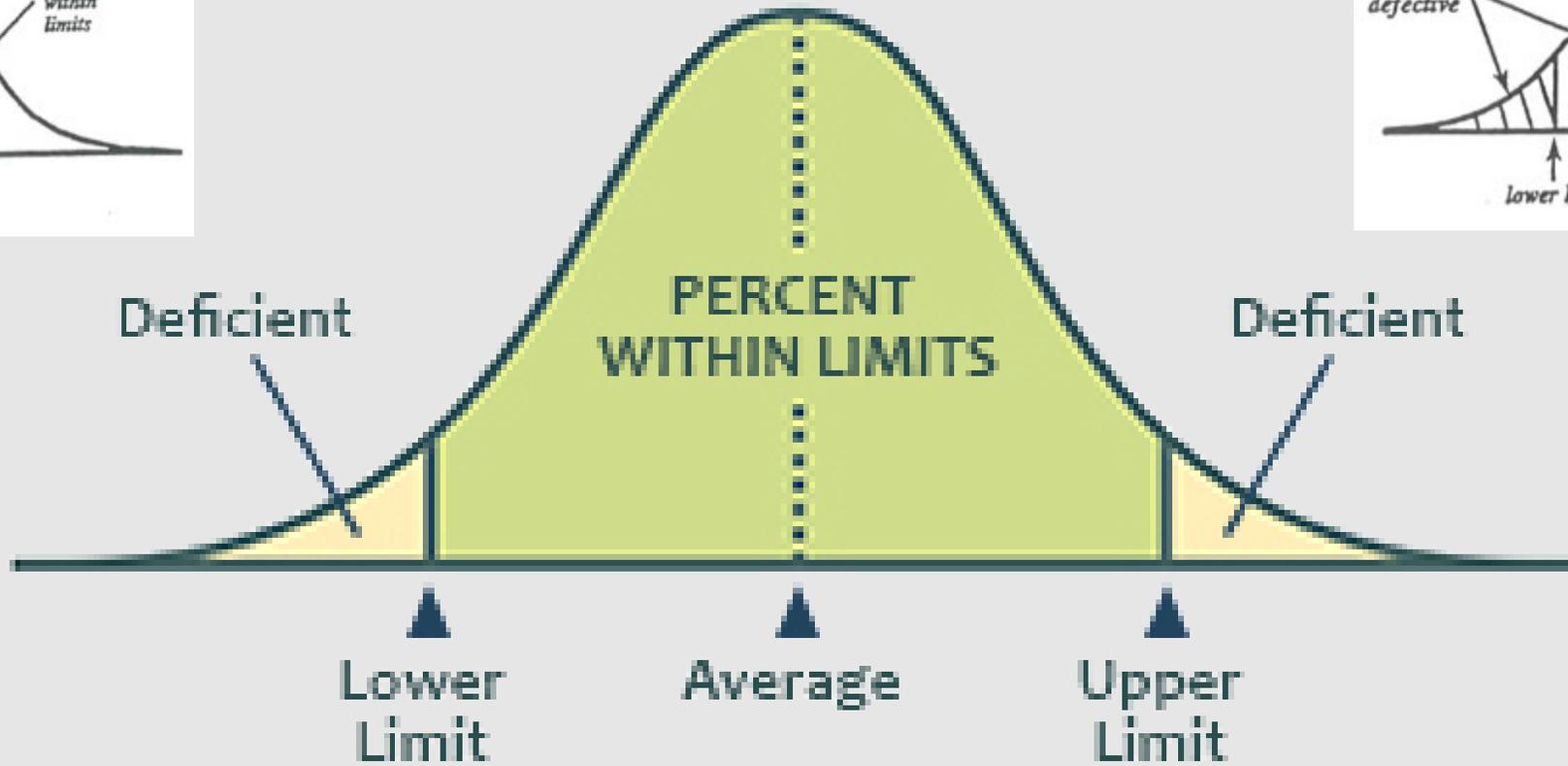
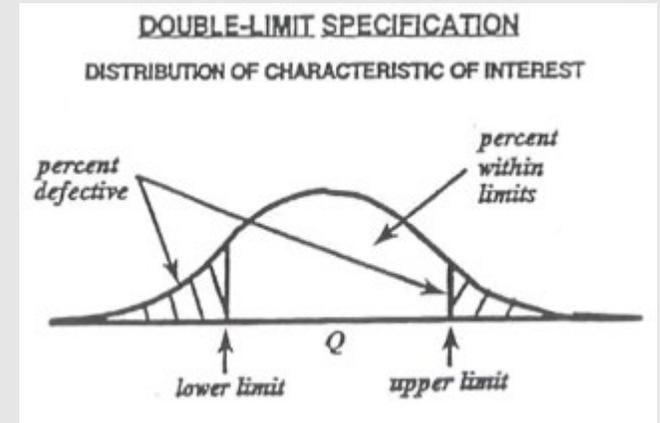
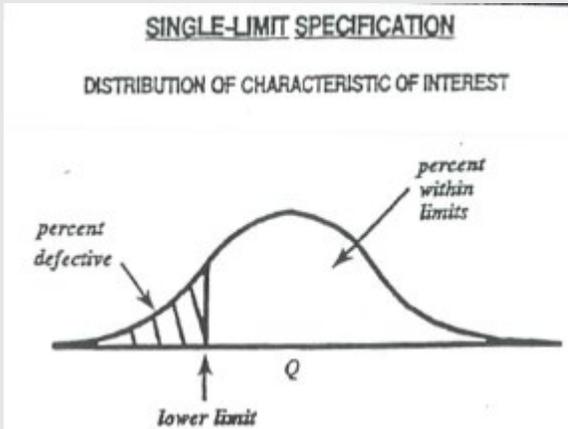




# Percent Within Limits Analysis and Performance



# Percent Within Limits Project Data



# Background

- A PWL value is calculated using lower limits for density (usually 93%) and lower and upper limits (2.0 and 4.3 respectively) for Air Voids.
- The PWL value is used in a pay equation to determine the Pay Factor (PF).
- Incentives and disincentives are calculated using \$65/ton with the ability to get up to 4% in incentives (PF = 104).
  - PF > 100: Incentive
  - PF = 100: No incentive or disincentive
  - PF < 100: Disincentive
  - PF = 50: Contract unit price is used instead of \$65/ton and paid at 50% or remove and replace.
  - Max possible incentive per ton is \$2.60 ( $\$65/\text{ton} * 0.04$ ) or \$1.30 each for density and air voids.

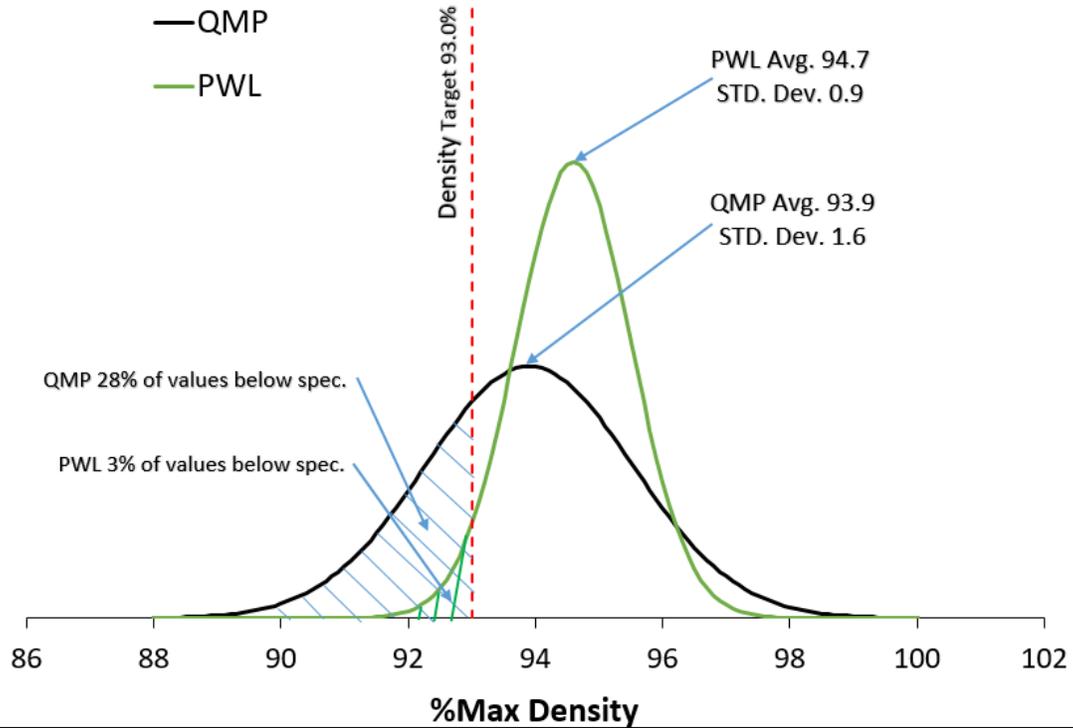


# What Does It All Mean?

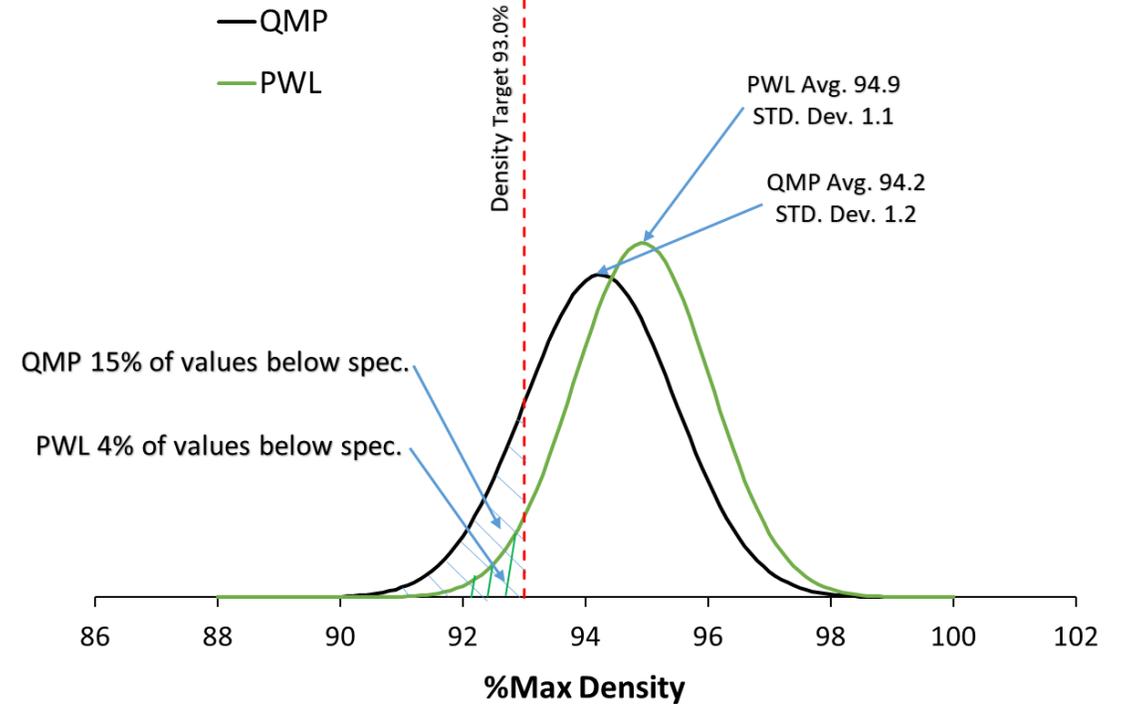
- Each of the improvements to the specification over the last decade have been instrumental in building better asphalt pavements.
  - Increased density = longer lasting pavements.
  - Additional asphalt = reduced cracking and aging.
  - PWL = more consistent, quality material.
  - Joint density testing = better performing joints.
- Overall: longer lasting pavements = greater return on investment

# Percent Within Limits

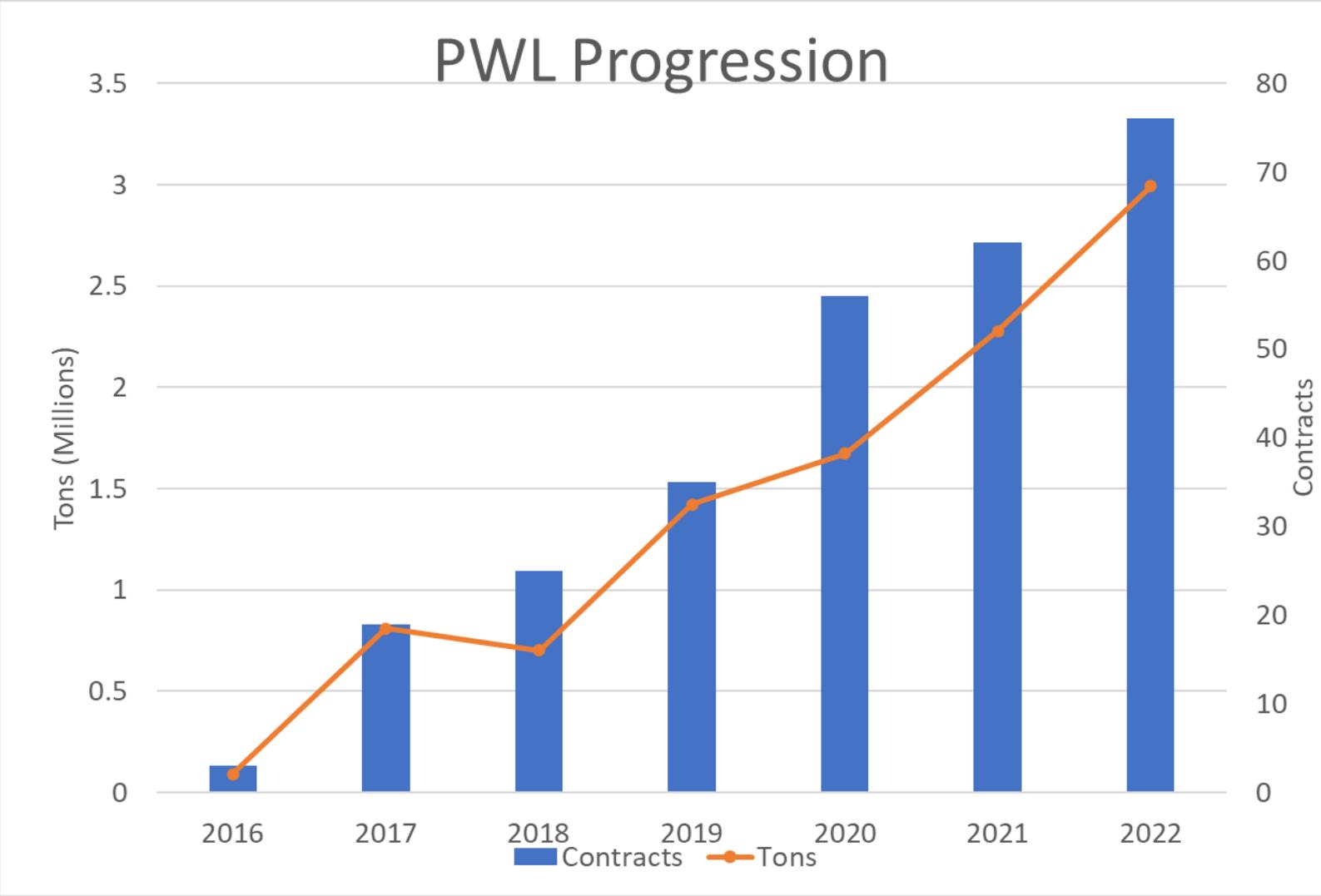
## 2017 Density Data



## 2018 Density Data



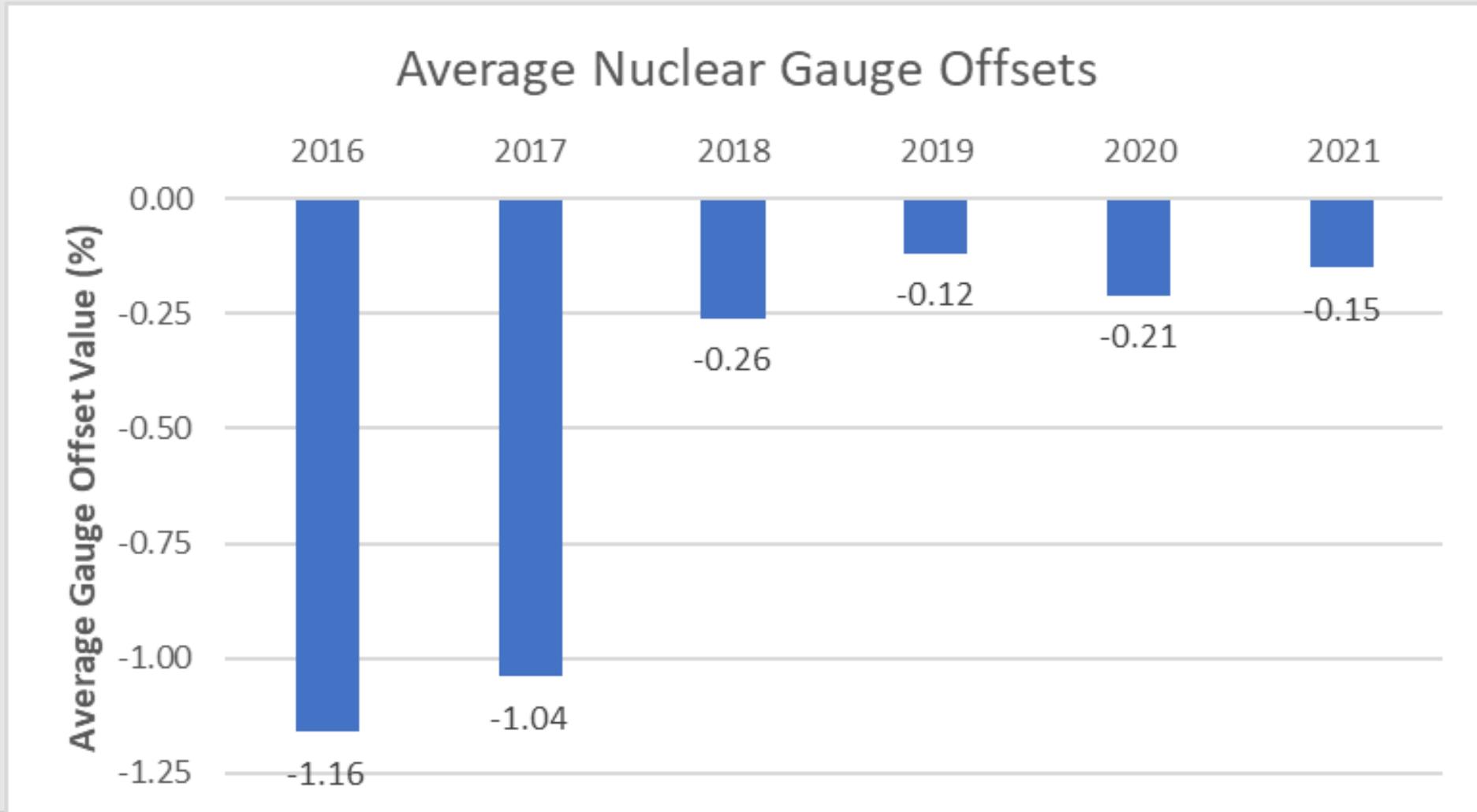
# PWL - Percent Within Limits



# PWL - Percent Within Limits

|                         | 2016 | 2017 | 2018 | 2019   | 2020                      | 2021                      | 2022                      |
|-------------------------|------|------|------|--------|---------------------------|---------------------------|---------------------------|
| Number of PWL Contracts | 3    | 19   | 25   | 35     | 56                        | 62                        | 76                        |
| Tons                    | 91K  | 811K | 701K | 1,423K | 1,673K<br>~55% of program | 2,278K<br>~65% of program | 2,994K<br>~63% of program |

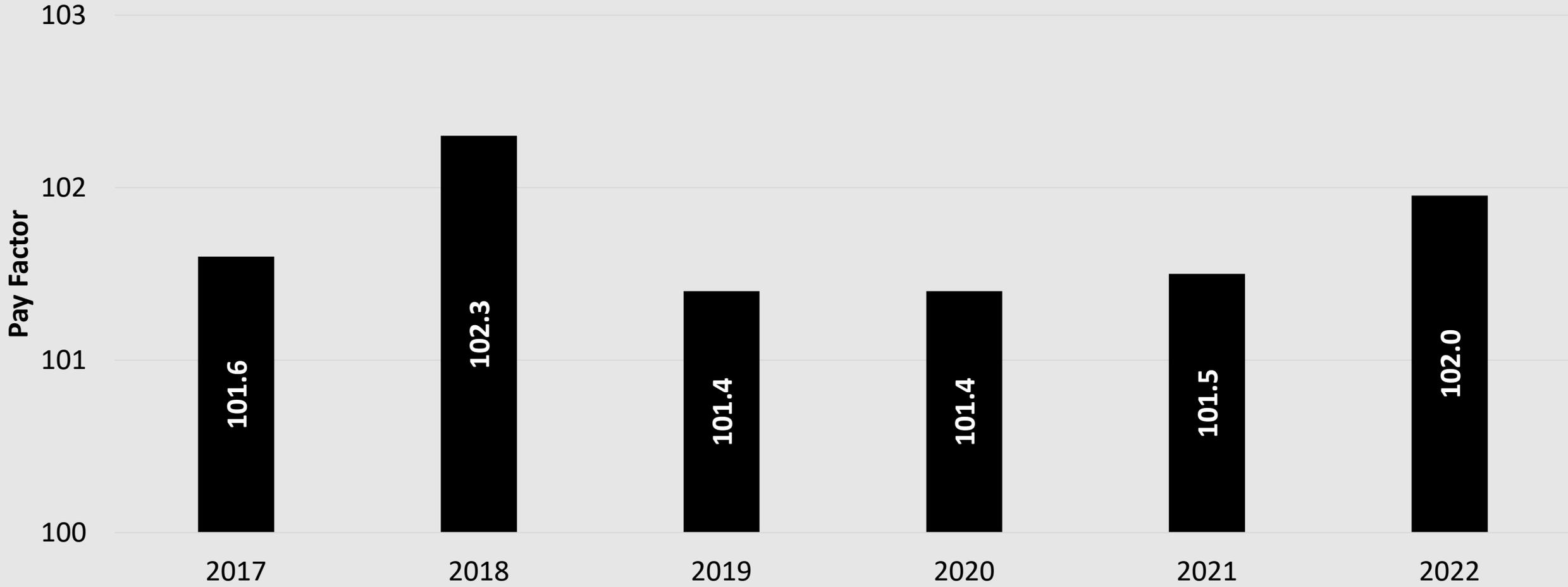
# Gauge offsets



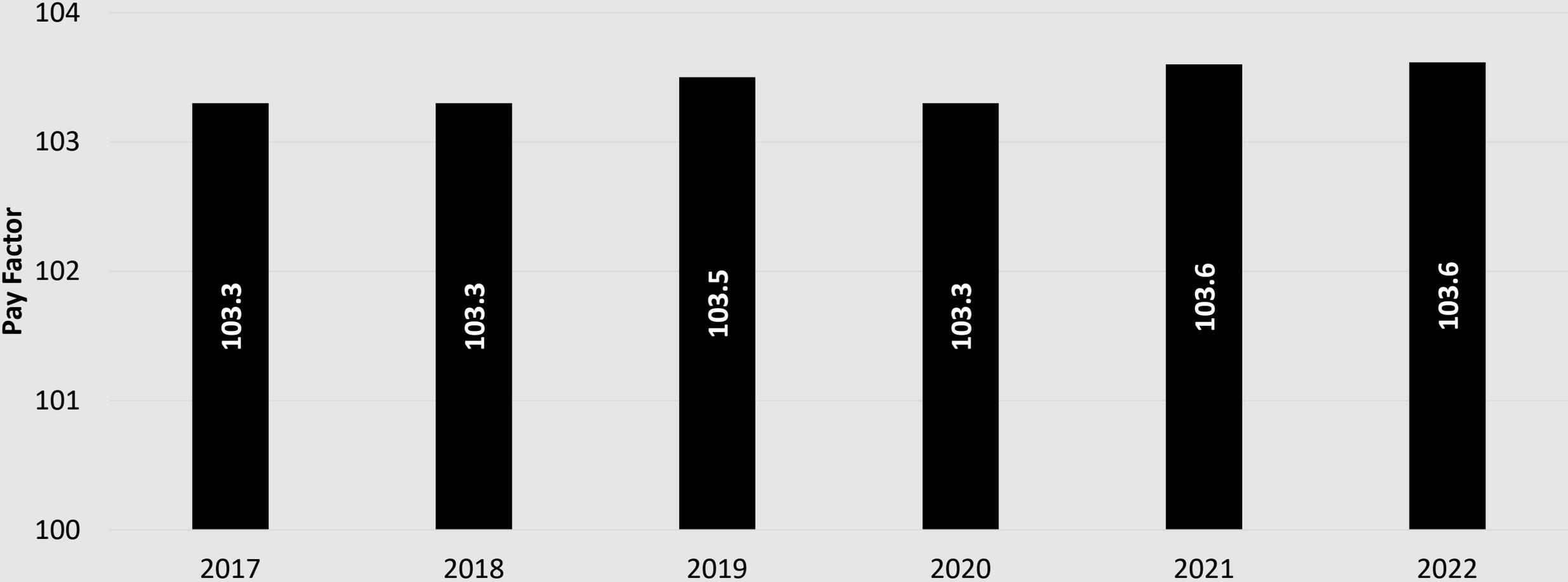
# 2022 PWL Data Review



# Average Annual Pay Factors - Density

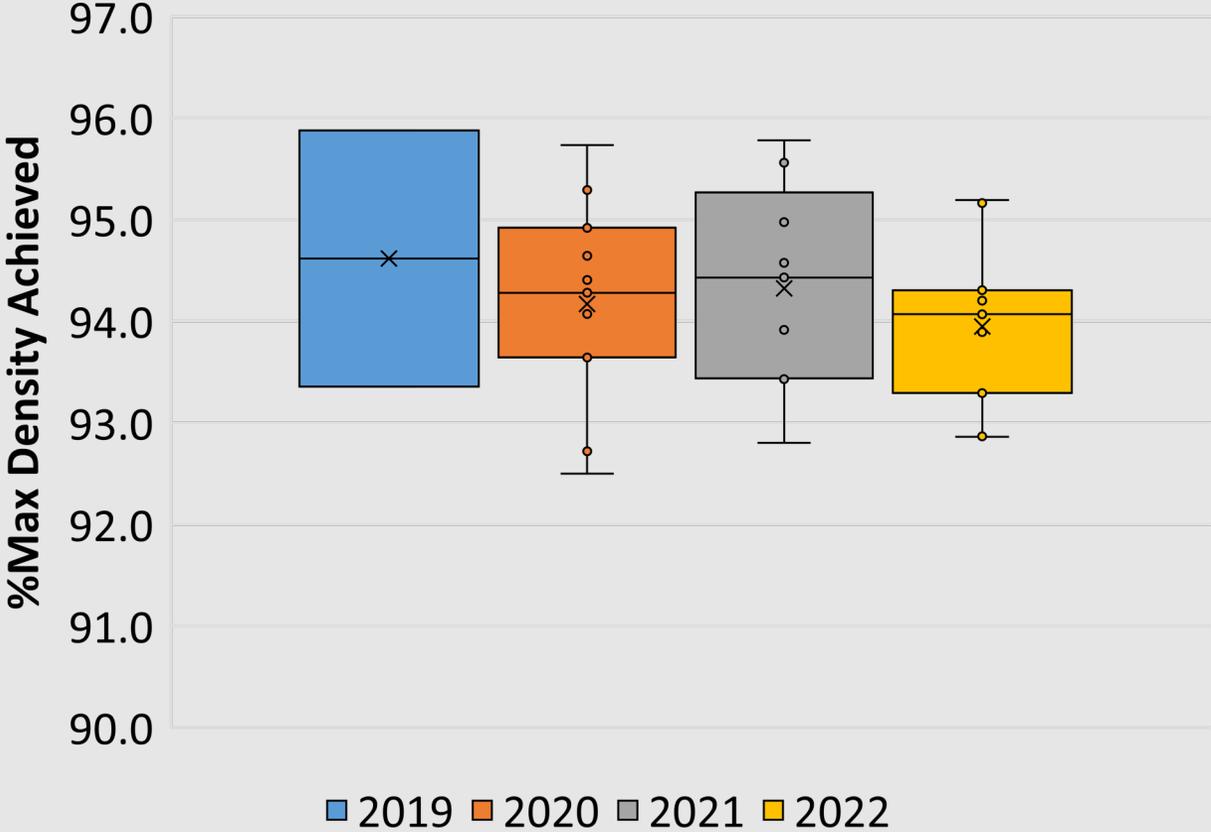


# Average Annual Pay Factors – Air Voids

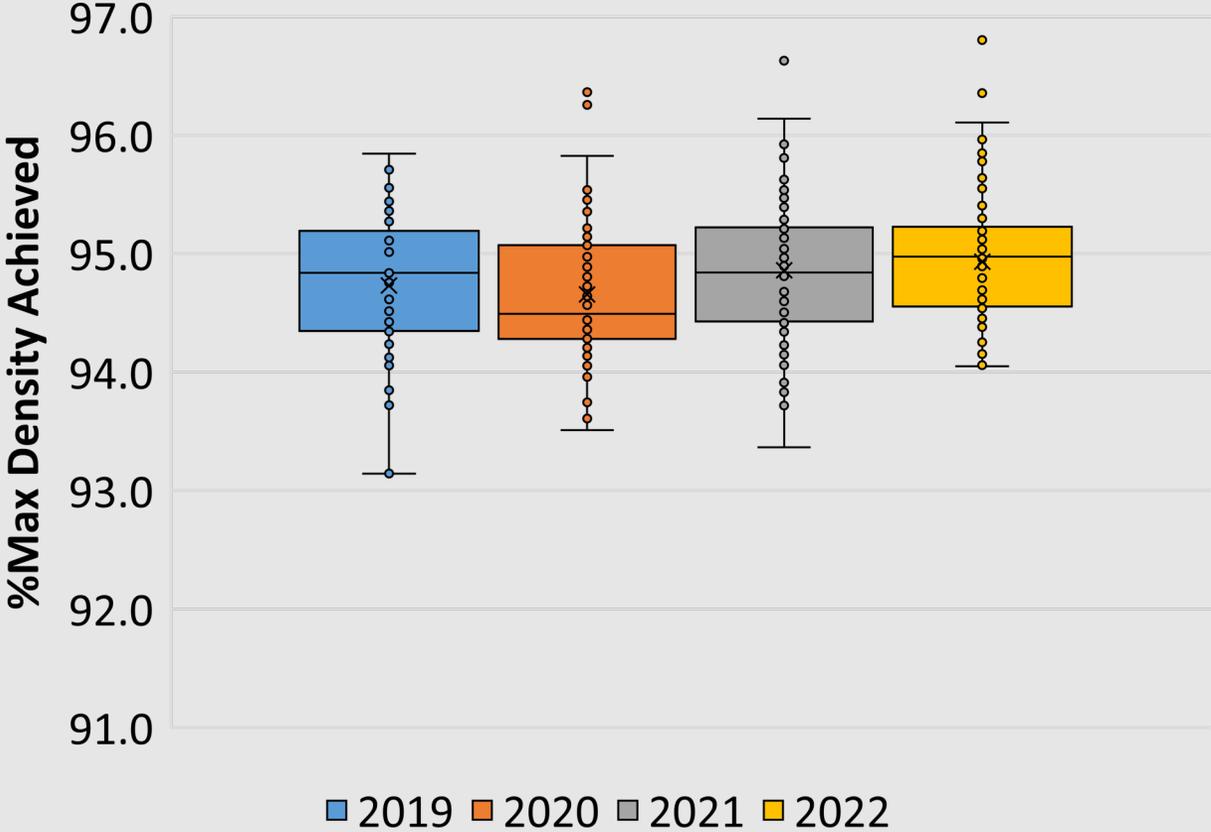


# Annual Density Distribution Comparison

Min. Req. of 91%

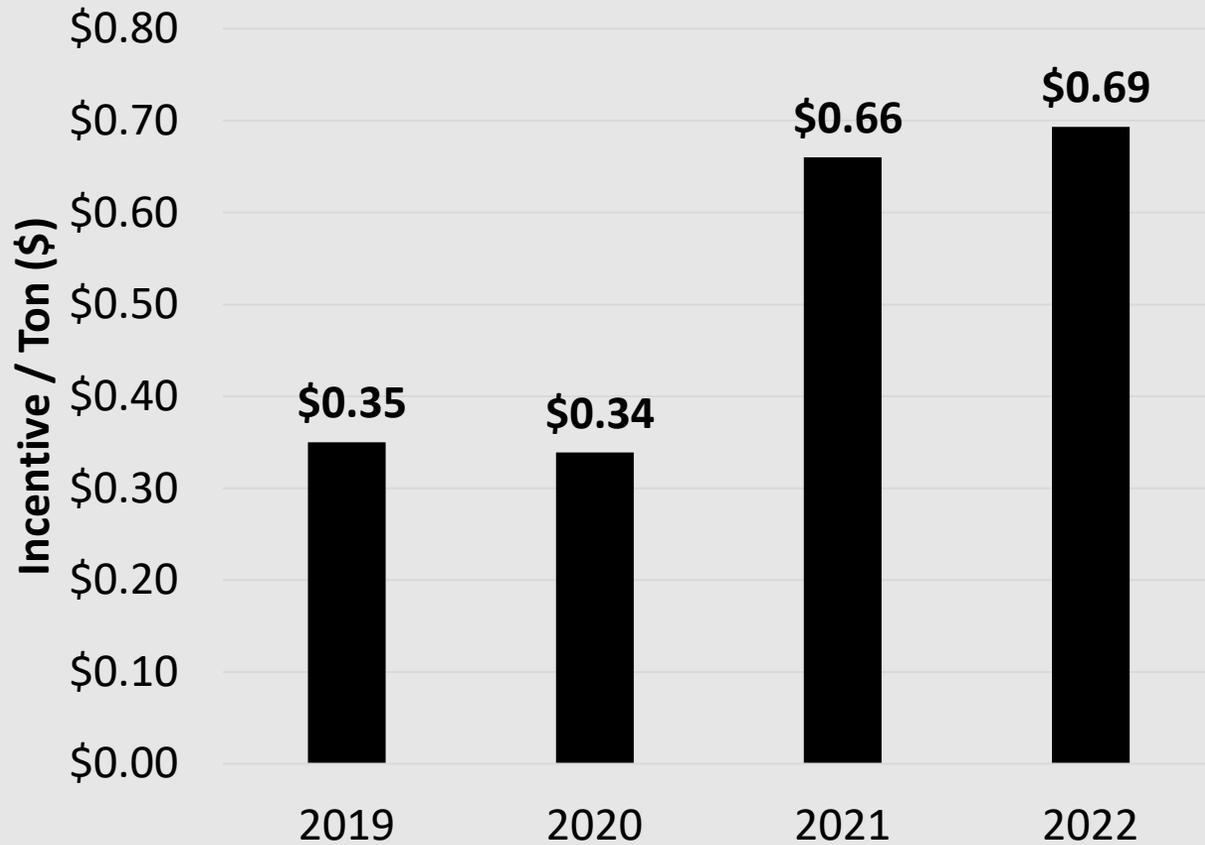


Min. Req. of 93%

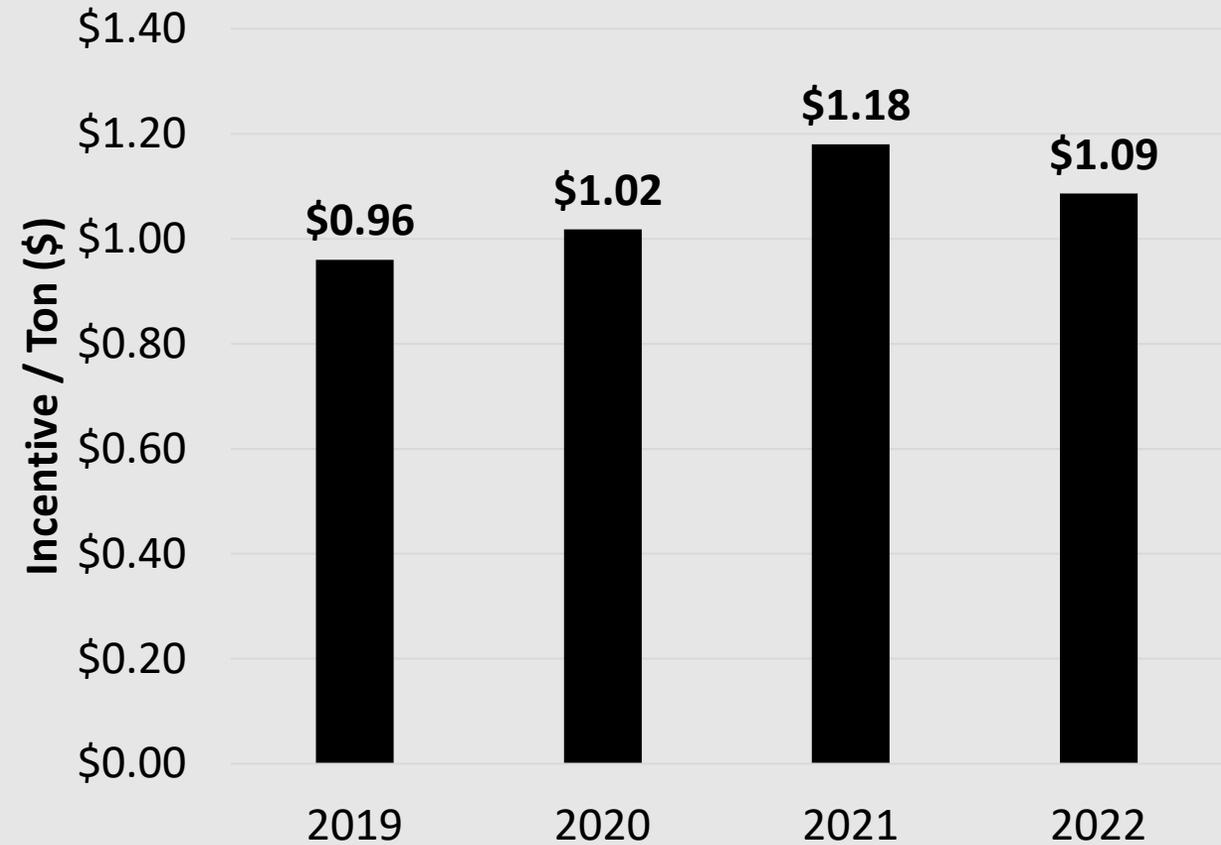


# Incentive / Ton

## Density



## Volumetrics (Va and AC)

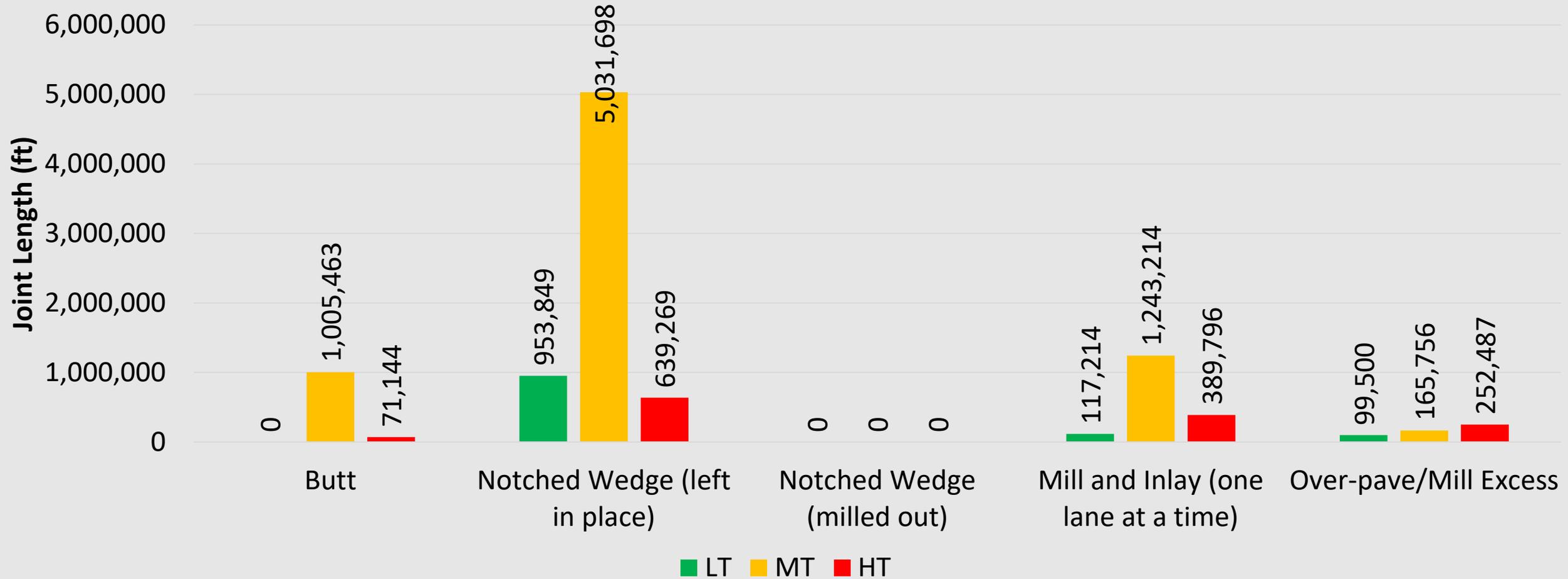




# Longitudinal Joint Density



# 1,888 Miles of Joint Length Paved!

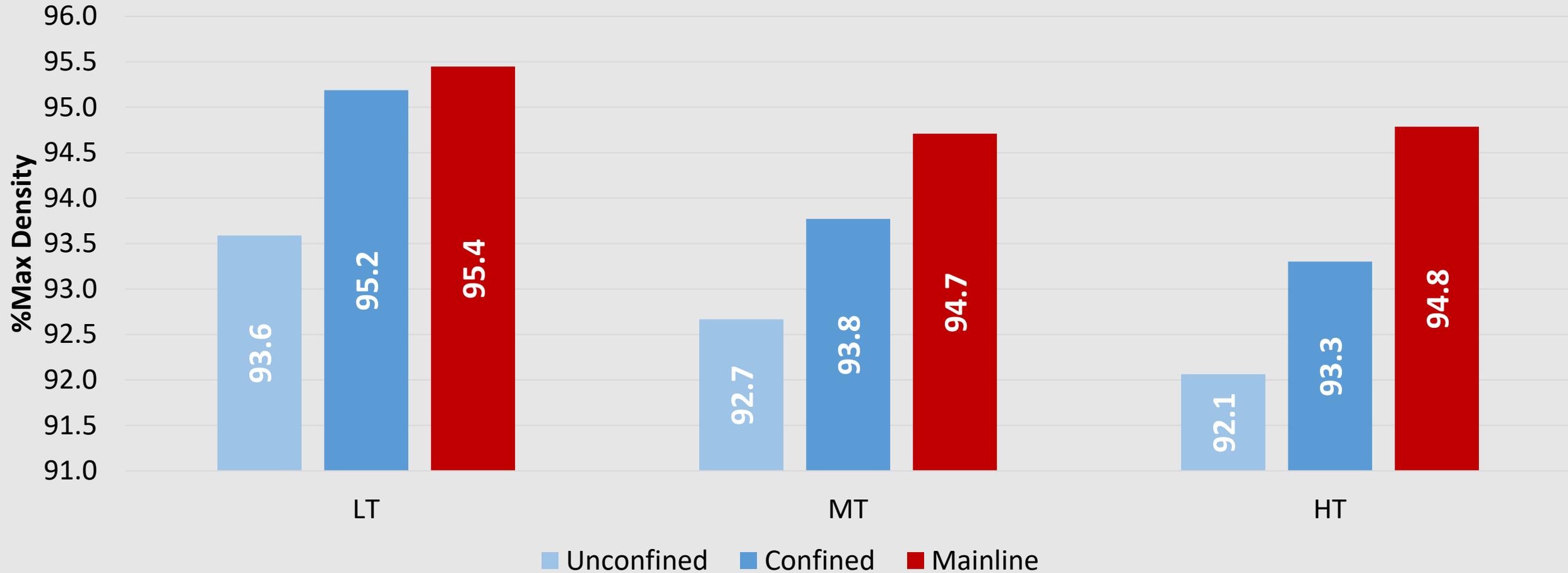


# Mill and Inlay and Over-Pave Mill Excess Earn the Most Incentive/LF!



# The Laws of Confinement

Unconfined < Confined < Mainline



# Tables

| Longitudinal Joint Density          |                    |                          |                |              |              |                |
|-------------------------------------|--------------------|--------------------------|----------------|--------------|--------------|----------------|
| Joint Type                          | Number of Projects | Total Possible Incentive | Incentive Paid | Joint Length | Incentive/LF | %Max Incentive |
| Butt                                | 19                 | \$430,642.80             | \$255,468.40   | 1,005,669.0  | \$0.25       | 59.3%          |
| Notched Wedge (left in place)       | 74                 | \$2,649,926.35           | \$2,109,929.81 | 6,035,502.7  | \$0.35       | 79.6%          |
| Notched Wedge (milled out)          | 0                  | \$-                      | \$-            | 0.0          | N/A          | N/A            |
| Mill and Inlay (one lane at a time) | 19                 | \$700,089.60             | \$521,493.60   | 1,449,354.0  | \$0.36       | 74.5%          |
| Over-pave/Mill Excess               | 7                  | \$207,097.20             | \$160,259.60   | 519,743.0    | \$0.31       | 77.4%          |
| Combined                            | 119                | \$3,987,755.95           | \$3,047,151.41 | 9,010,268.7  | \$0.34       | 76.4%          |



# Background – Density Pay Factor Table

| Average Density (%)       | Pay Factor  |            |            |            |            |            |            |            |
|---------------------------|-------------|------------|------------|------------|------------|------------|------------|------------|
| <b>96.0</b>               | 104.00      | 104.00     | 104.00     | 104.00     | 104.00     | 104.00     | 103.91     | 103.60     |
| <b>95.5</b>               | 104.00      | 104.00     | 104.00     | 104.00     | 104.00     | 103.91     | 103.51     | 102.77     |
| <b>95.0</b>               | 104.00      | 104.00     | 104.00     | 104.00     | 103.91     | 103.35     | 102.33     | 101.10     |
| <b>94.5</b>               | 104.00      | 104.00     | 104.00     | 103.91     | 103.05     | 101.52     | 99.83      | 97.91      |
| <b>94.0</b>               | 104.00      | 104.00     | 103.91     | 102.33     | 99.83      | 97.04      | 94.79      | 92.99      |
| <b>93.5</b>               | 104.00      | 103.91     | 99.83      | 94.79      | 91.56      | 89.43      | 87.94      | 86.85      |
| <b>93.0</b>               | 80.00       | 80.00      | 80.00      | 80.00      | 80.00      | 80.00      | 80.00      | 80.00      |
| <b>92.5</b>               | 50.00       | 50.00      | 50.00      | 50.00      | 50.00      | 50.00      | 50.00      | 50.00      |
| <b>92.0</b>               | 50.00       | 50.00      | 50.00      | 50.00      | 50.00      | 50.00      | 50.00      | 50.00      |
| <b>Standard Deviation</b> | <b>0.05</b> | <b>0.2</b> | <b>0.4</b> | <b>0.6</b> | <b>0.8</b> | <b>1.0</b> | <b>1.2</b> | <b>1.4</b> |



# Background – Air Voids Pay Factor Table

| Average Air Voids         | Pay Factor  |            |            |            |            |            |            |            |            |
|---------------------------|-------------|------------|------------|------------|------------|------------|------------|------------|------------|
| 4.3                       | 80.00       | 80.00      | 80.00      | 80.00      | 80.00      | 80.00      | 80.00      | 50.00      | 50.00      |
| 4.2                       | 103.99      | 87.83      | 83.94      | 82.63      | 81.98      | 81.58      | 80.53      | 80.53      | 50.00      |
| 4.0                       | 104.00      | 101.04     | 91.58      | 87.83      | 85.90      | 84.71      | 81.86      | 81.86      | 50.00      |
| 3.8                       | 104.00      | 104.00     | 98.41      | 92.79      | 89.72      | 86.81      | 82.84      | 82.84      | 50.00      |
| 3.6                       | 104.00      | 104.00     | 102.89     | 97.36      | 93.38      | 88.15      | 83.52      | 83.52      | 50.00      |
| 3.4                       | 104.00      | 104.00     | 104.00     | 101.04     | 95.43      | 88.94      | 83.94      | 83.94      | 80.13      |
| 3.2                       | 104.00      | 104.00     | 104.00     | 103.36     | 96.21      | 89.27      | 84.12      | 84.12      | 80.24      |
| 3.0                       | 104.00      | 104.00     | 104.00     | 102.33     | 95.95      | 89.17      | 84.06      | 84.06      | 80.20      |
| 2.8                       | 104.00      | 104.00     | 103.99     | 99.42      | 94.61      | 88.61      | 83.76      | 83.76      | 80.02      |
| 2.6                       | 104.00      | 104.00     | 101.04     | 95.14      | 91.58      | 87.55      | 83.21      | 83.21      | 50.00      |
| 2.4                       | 104.00      | 103.99     | 95.14      | 90.35      | 87.83      | 85.89      | 82.39      | 82.39      | 50.00      |
| 2.2                       | 104.00      | 95.14      | 87.83      | 85.25      | 83.94      | 83.16      | 81.25      | 81.25      | 50.00      |
| 2.0                       | 80.00       | 80.00      | 80.00      | 80.00      | 80.00      | 80.00      | 80.00      | 50.00      | 50.00      |
| <b>Standard Deviation</b> | <b>0.05</b> | <b>0.2</b> | <b>0.4</b> | <b>0.6</b> | <b>0.8</b> | <b>1.0</b> | <b>1.2</b> | <b>1.2</b> | <b>1.4</b> |



# Where are we headed?

- PWL Lite for lower tonnages
- PWL for SMA
- PWL for Asphalt Content



# New HMA QAP Programs

(Replacement for QMP program)



# Disclaimer

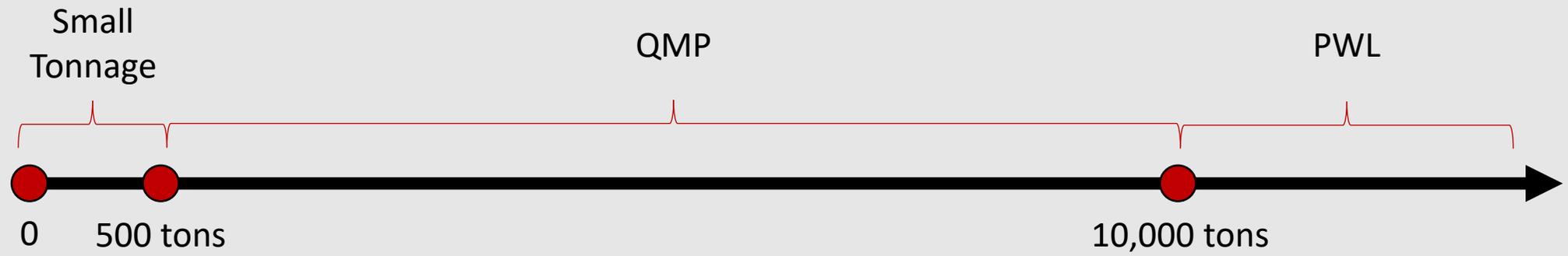
- The concepts presented herein are still works in progress and are subject to change before the final rollout of the new AWP reorganized specifications.



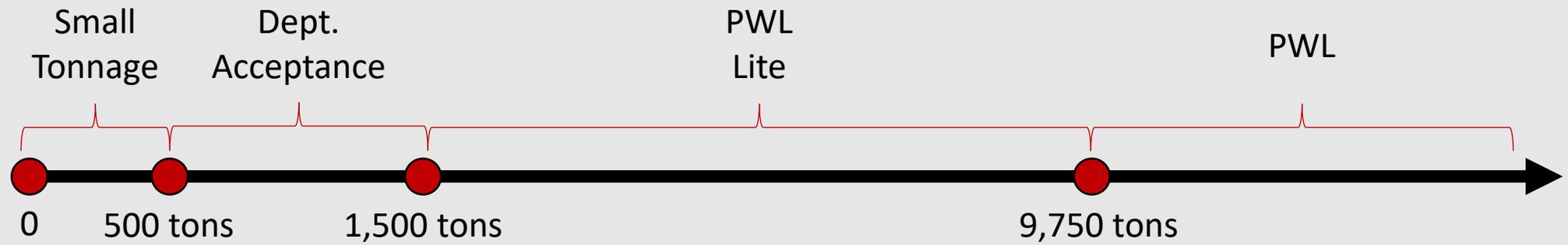
# Mixture / Volumetric Testing



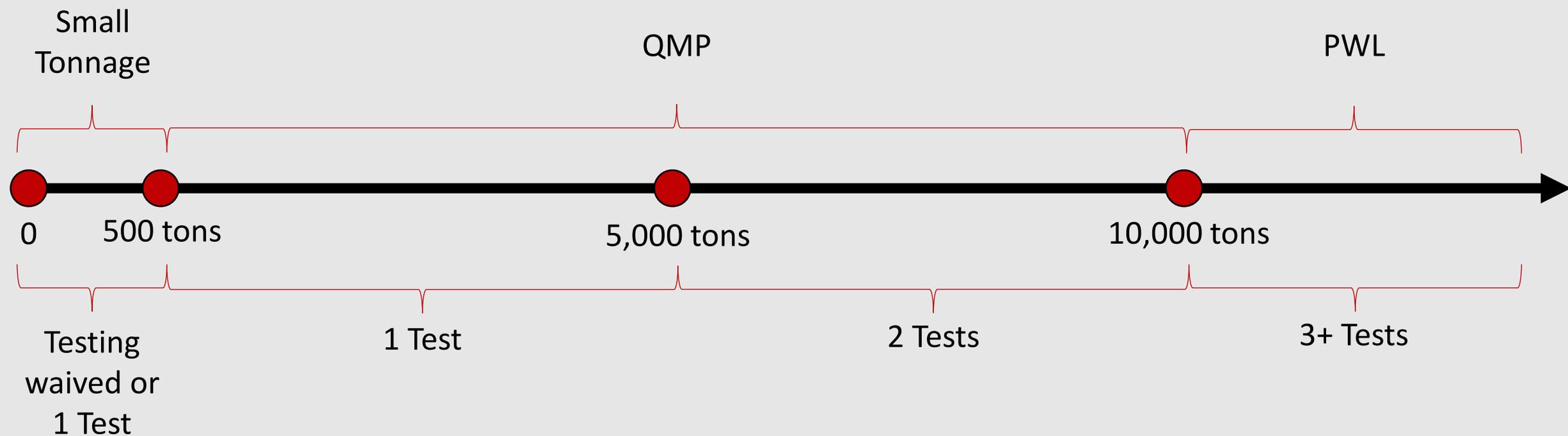
# Existing QMP



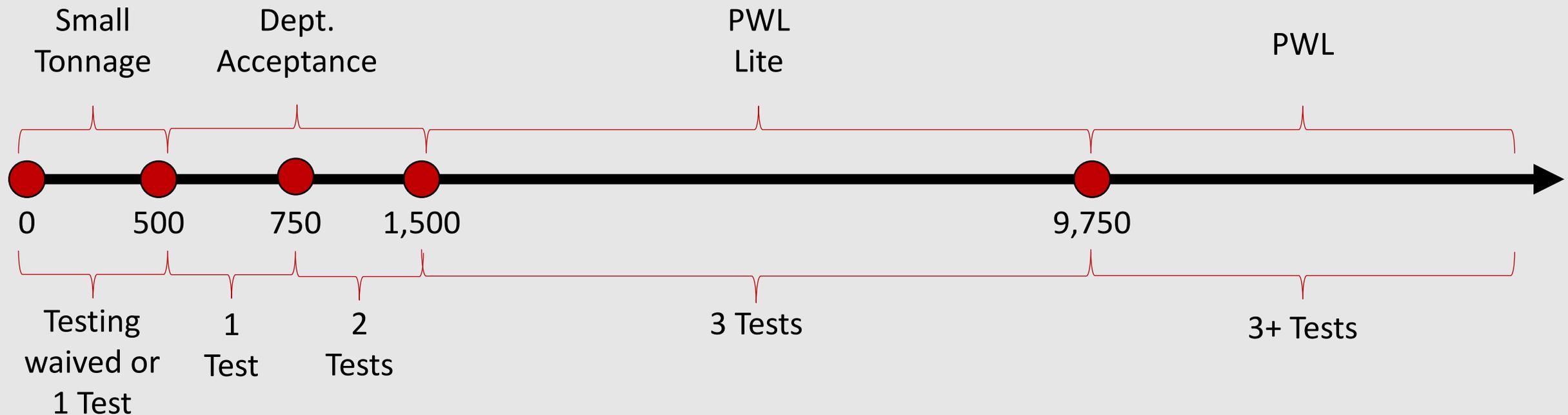
# New QAPs



# Existing QMP QV Testing Breakdown



# New QAP QV Testing Breakdown



# Density Testing

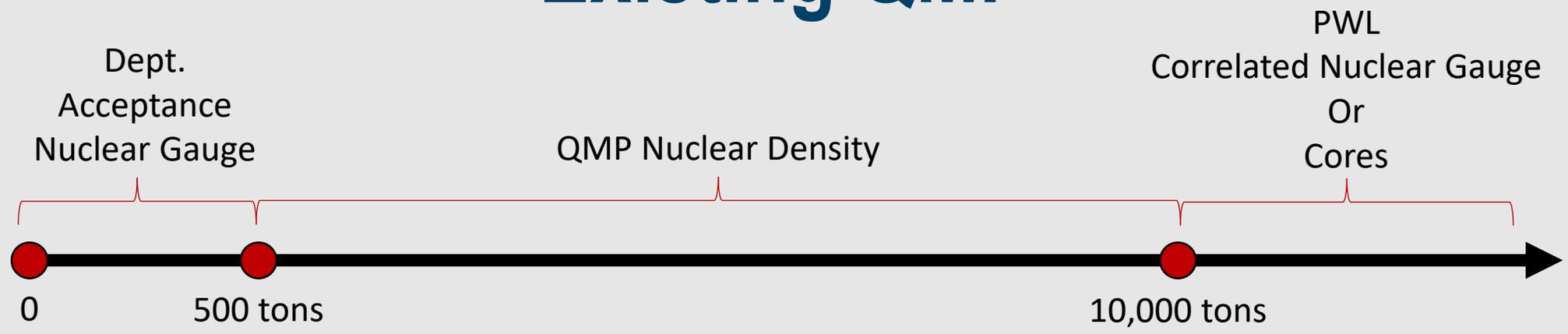


# Density / Correlation Test Strips

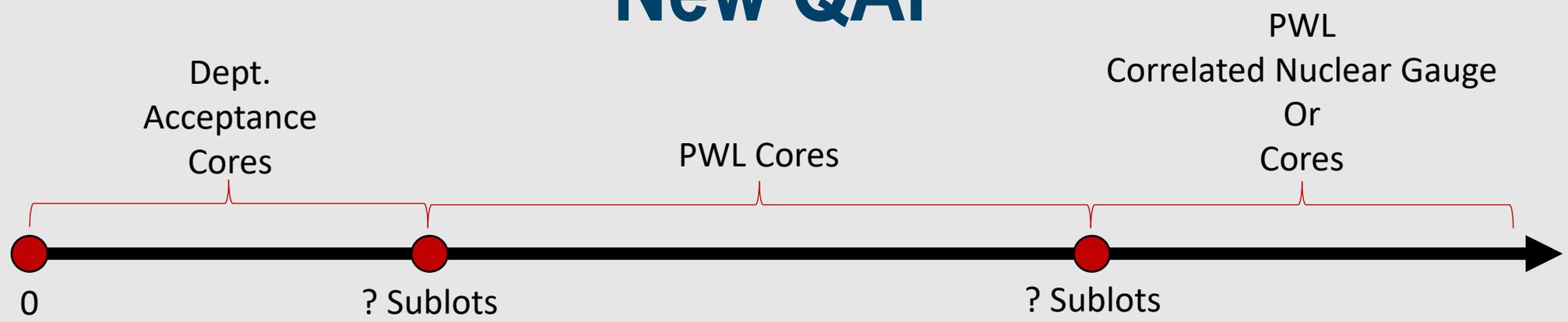
- **ONLY** required for correlation purposes **when** using a nuclear gauge.
  - Density Correlation/Test Strips to be either 2 density sublots (3,000 LF) or 750 tons.
    - Use 750 tons when performing combined volumetric/density test strip.
    - Use 2 sublots otherwise.



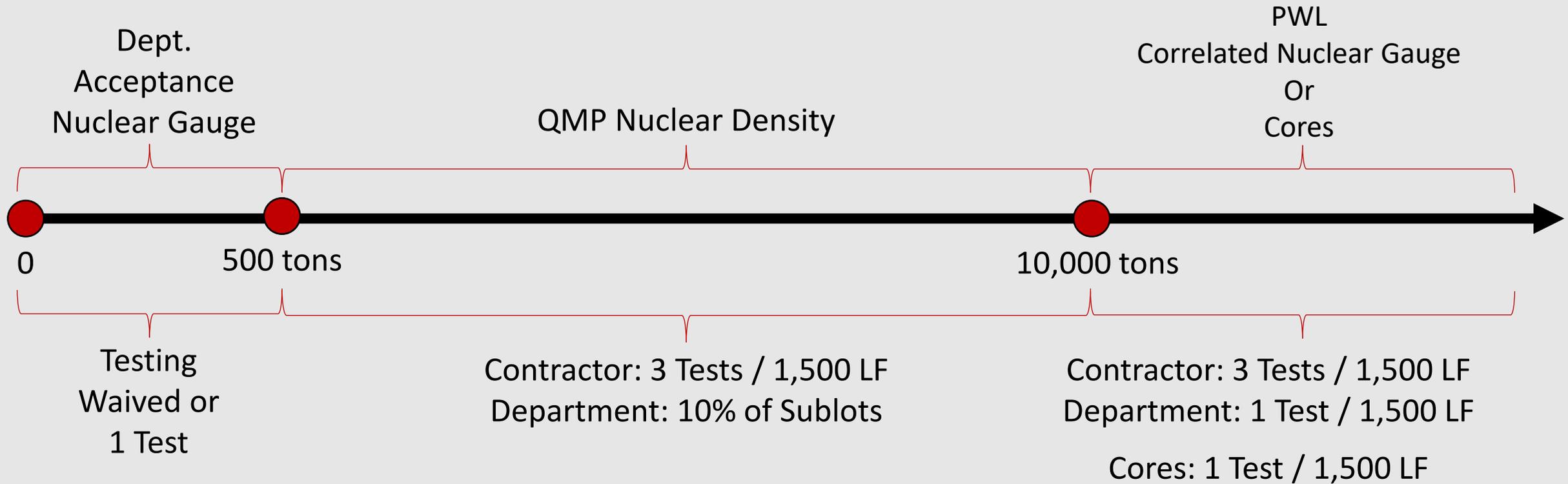
# Existing QMP



# New QAP

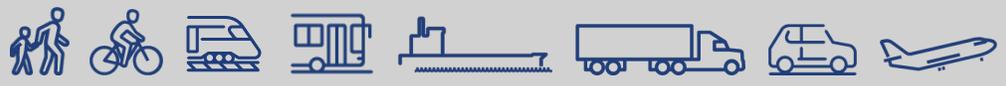
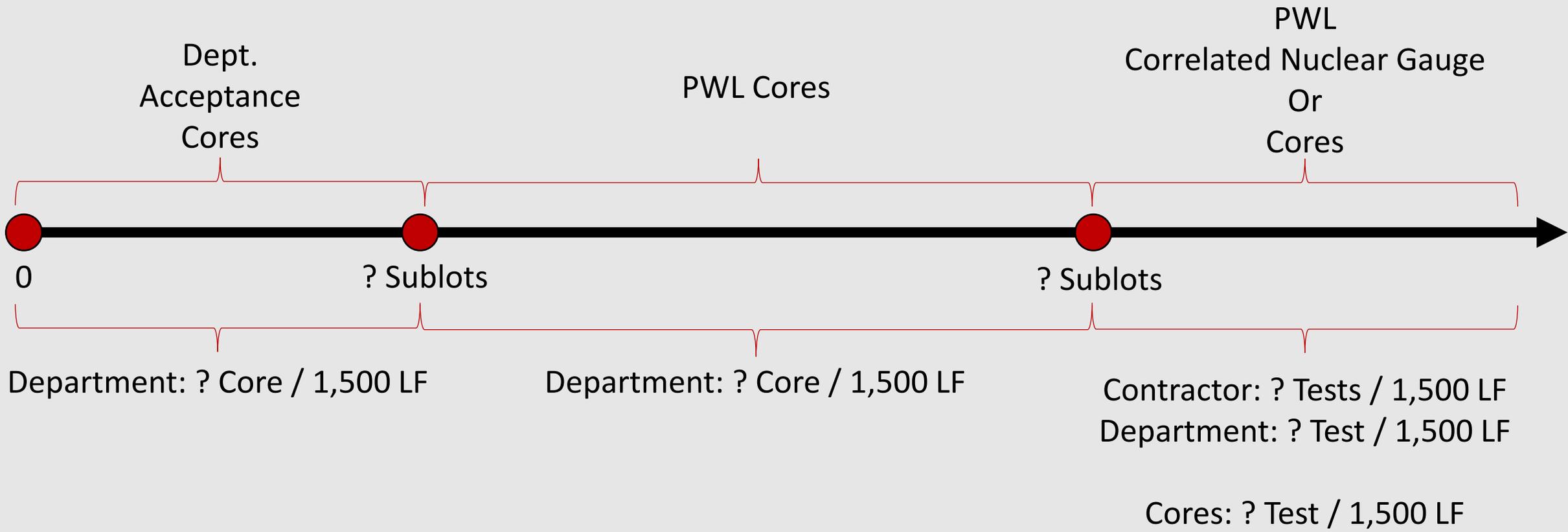


# QMP Density Testing Breakdown





# New Density Testing Breakdown



# PWL for SMA

- PWL for SMA
- Review F&t analysis
  - Review potential for additional dispute resolution
- Review air void targets
  - +/-1.3 from 4.5% target? (3.2 – 5.7%)



# PWL for Asphalt Content

- PWL for Asphalt Content
  - % Binder or VMA
- Review F&t analysis
  - Review potential for additional dispute resolution
- Review targets
  - -0.3% below JMF



# BMD:

## An Update on WisDOT's Current Practice and Future Plans

**Ali Arabzadeh, PhD, PE**



# BMD: a method for increasing the durability of asphalt mixtures in WI

- Balanced Mix Design (BMD)

- What is BMD?

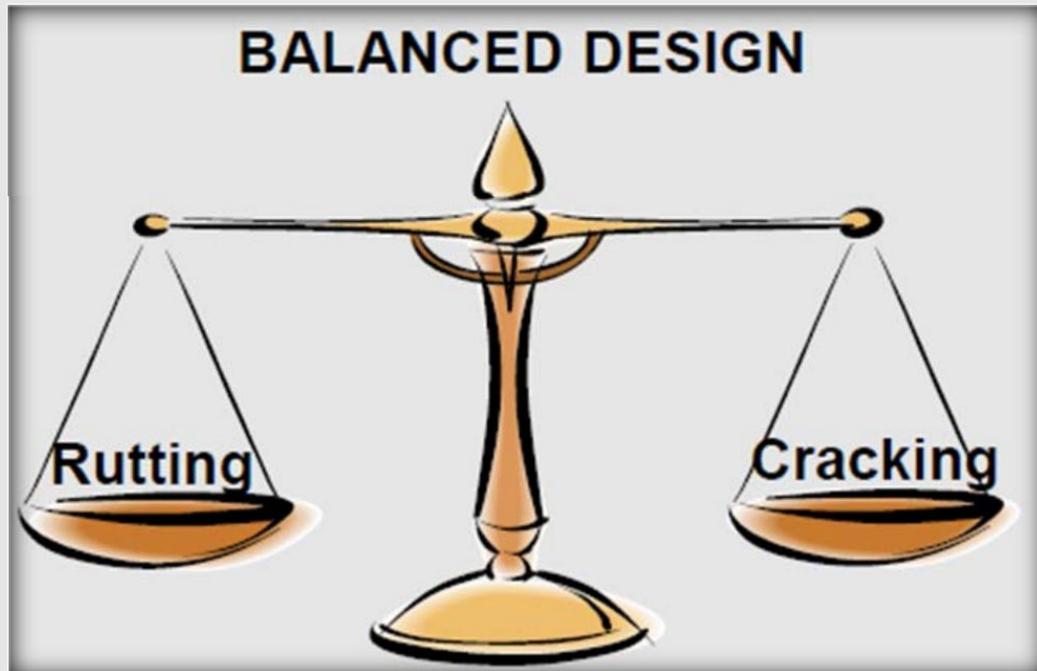
- According to Federal Highway Administration (FHWA) Expert Task Group (ETG) BMD Task Force, BMD is “*asphalt mix design using performance tests on appropriately conditioned specimens that address multiple modes of distress taking into consideration mix aging, traffic, climate and location within the pavement structure.*”

- Why do we need BMD?

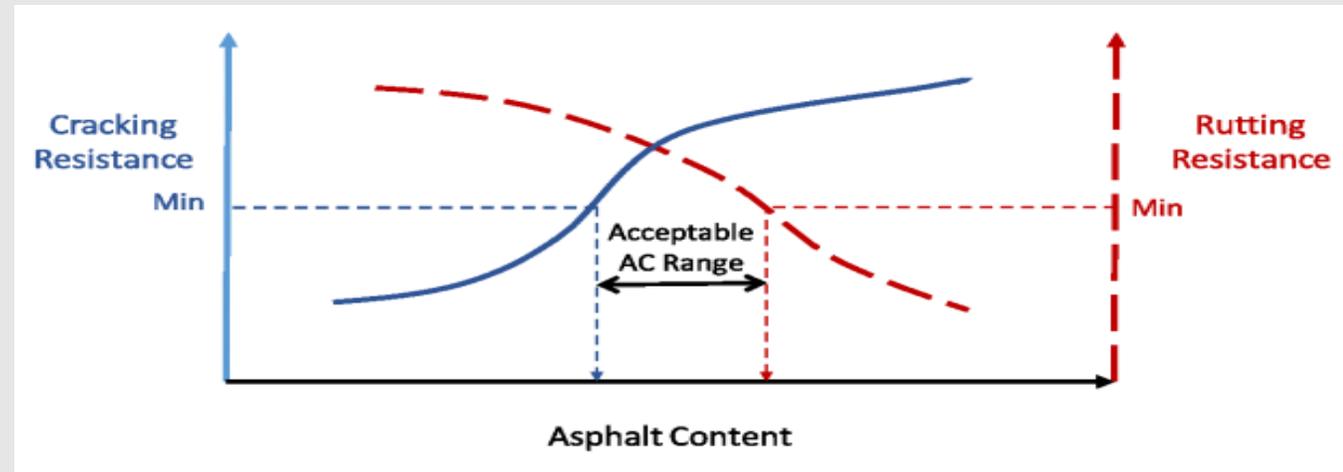
- Ensure performance
    - Enable innovation
    - Enable economic optimization

# BMD: a method for increasing the durability of asphalt mixtures in WI

- BMD concept
  - A balance between cracking and rutting resistance



Buchanan, 2017



Newcomb et al., 2018



Buchanan, 2017

# BMD: a method for increasing the durability of asphalt mixtures in WI

- BMD approaches (currently investigating the appropriateness of Approach A)
  - **Approach A: Volumetric Design with Performance Verification**
    - Starts with an agency approved mix design
    - The mix design is tested with selected mixture rutting and cracking tests
    - If the mix design is failed, the entire mix design is repeated until all the volumetric and performance test criteria are satisfied
  - **Approach B: Volumetric Design with Performance Optimization**
    - Similar to approach A, except for
    - Testing the performance at OBC and two or more additional binder contents of  $\pm 0.3$  to  $0.5\%$
    - Selecting a binder content that satisfies the performance criteria

# BMD: a method for increasing the durability of asphalt mixtures in WI

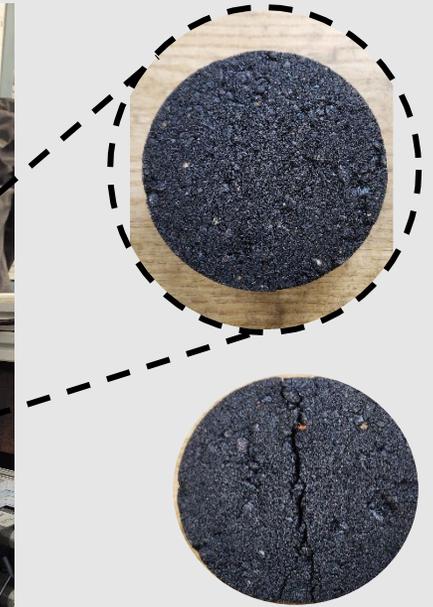
- BMD approaches (currently investigating the appropriateness of Approach A)
  - **Approach C: Performance-Modified Volumetric Design**
    - Similar to approach A, except for
    - Adjusting the binder content or other mix component properties such as aggregates, binders, recycled materials, and additives.
    - Making sure that certain volumetric properties are in compliance with agency's relaxed requirements
  - **Approach D: Performance Design**
    - An existing agency-approved mix design is used
    - The mix design is tested with selected mixture rutting and cracking tests at three or more binder contents at intervals of 0.3 to 0.5 %
    - A binder content that satisfies both the rutting and cracking criteria is selected as the OBC

# BMD Performance Tests Used in WI

- There are many different types of performance tests
- WisDOT uses:
  - Hamburg wheel tracking test (HWTT)
  - Indirect tensile asphalt cracking Test (IDEAL-CT)



HWTT @ 46° C



IDEAL-CT @ 25° C

# BMD Implementation Train is Unstoppable ...

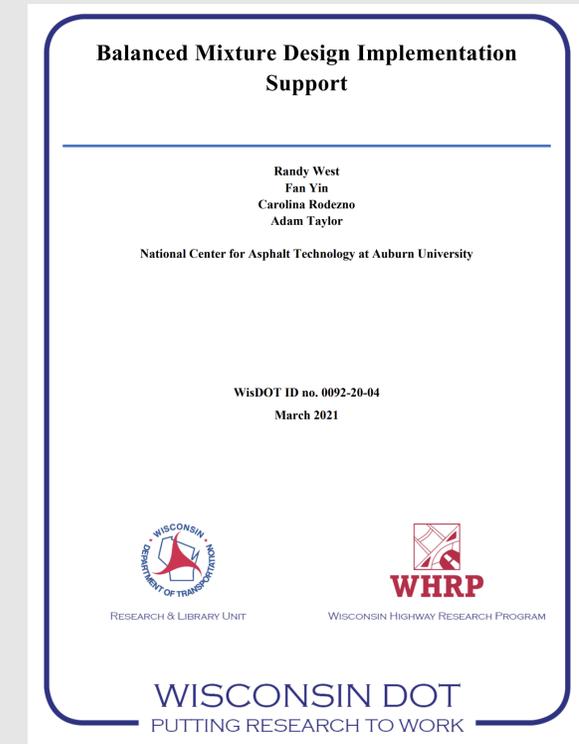
- We have invested substantially and will continue to do so
  - External research
    1. Balanced Mixture Design Implementation Support (status: completed in May 2021)
    2. Balanced Mixture Design Pilot and Field Test Sections (status: under review by WHRP\* Flexible Pavements TOC\*)
      - \$5,000,000 has been spent on BMD-related research!
      - We will have an upcoming WHRP research focusing on Approach C
  - In-house research
    - BMD Benchmarking Experiment
      - WisDOT's Central Office has been investigating the suitability of BMD implementation for about **4 years!**
      - Next step is field validation
- In the future, it can be a tool for justifying the sustainability of unsustainable materials used at the plant
- There will be challenges ...
  - We are committed to collaborate with the regions and industry to make the transition as **smooth** as possible

\*Note: WHRP and TOC are the abbreviations of Wisconsin Highway Research Program and Technical Oversight Committee.



# External Research Project No.1

- *Balanced Mixture Design Implementation Support* (status: completed in May 2021)
  - A benchmarking experiment was conducted by NCAT\* researchers to establish preliminary performance criteria
  - 18 Total mix designs were tested.
    - Thirteen 12.5-mm mixes
      - Three HT Mixes (PG 58-28S)
      - Five MT Mixes (PG 58-28S)
      - Four LT Mixes (PG 58-28S)
      - One SMA (PG 58-28V)
    - Five 9.5-mm mixes
      - Four MT Mixes (3 - PG 58-28S and 1 - PG 52-34S)
      - One LT Mix (PG 58-28S)



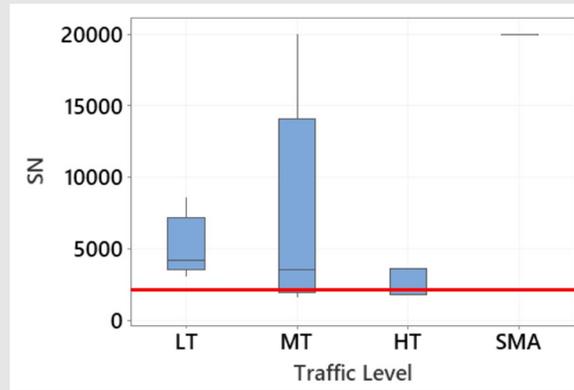
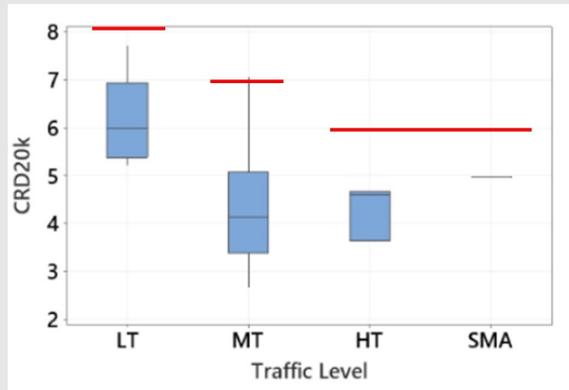
<https://wisconsindot.gov/documents2/research/0092-20-04-final-report.pdf>

\*Note: NCAT is the abbreviation for National Center for Asphalt Technology.



# External Research Project No. 1

- The NCAT researchers suggested preliminary performance criteria:
  - HWTT
    - Since rutting has not been a problem for Wisconsin, the  $CRD^*_{20k}$  criteria were selected such that nearly all mixes in the benchmarking experiment pass the respective criteria
      - Based upon a rounded maximum value from the results for each traffic level
      - HT and SMA criteria were slightly relaxed from the maximum value due to uncertainty from the small datasets for these traffic levels (15 - 25% higher than the observed maximum value)
    - A minimum of 2,000 passes was suggested for  $SN^*$  for all mixes based on the findings of Yin et al. (2020), which indicated that the threshold successfully discriminated asphalt mixes with and without moisture damage



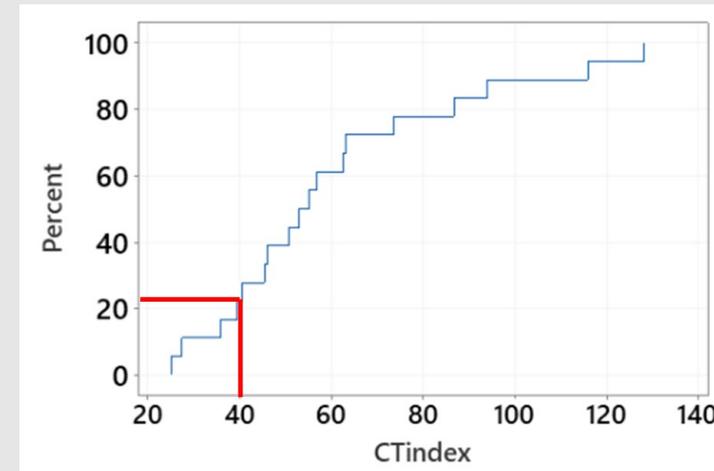
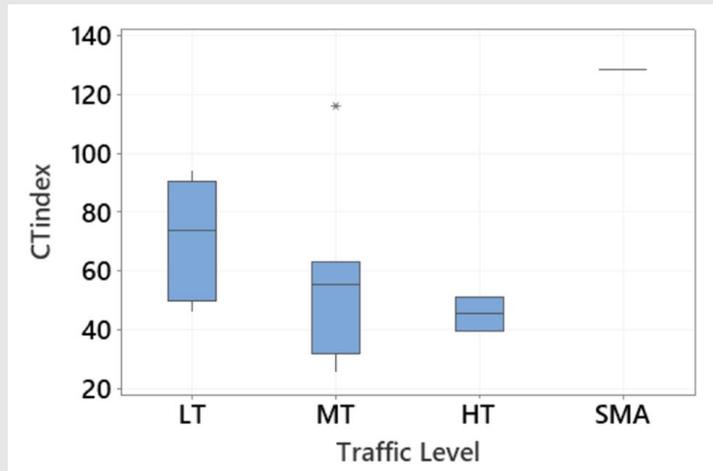
| Traffic Level | HWTT*            |               |
|---------------|------------------|---------------|
|               | $CRD_{20k}$ (mm) | $SN$ (passes) |
| SMA Mix       | $\leq 6.0$       | $\geq 2,000$  |
| HT Mix        | $\leq 7.0$       |               |
| MT Mix        | $\leq 7.0$       |               |
| LT Mix        | $\leq 8.0$       |               |

<https://wisconsin.gov/documents2/research/0092-20-04-final-report.pdf>

\*Note: CRD and SN are the abbreviations of corrected rut depth and stripping number.

# External Research No. 1

- The NCAT researchers suggested preliminary performance criteria:
  - **IDEAL-CT**
    - Different traffic levels are designed with different  $N_{design}$ , which results in different asphalt binder contents.
    - $CT^*_{Index}$  is highly dependent on the asphalt binder content of the mix
    - A minimum  $CT_{Index}$  of 40 was suggested for all traffic levels (LT, MT, HT)
      - Based upon the 25th percentile (40.4 CTIndex) of all mixtures benchmarked
    - SMA criteria was set at 80 CTIndex to ensure superior cracking resistance as a premium asphalt mixture



<https://wisconsin.gov/documents2/research/0092-20-04-final-report.pdf>

\*Note: CT is the abbreviation of cracking tolerance.



# External Research No. 2

- For part 2 of the research, the NCAT researchers obtained loose mixes from 10 shadow projects
  - To obtain representative data
- Mixes represent the state's diversity in aggregate type, binder grades, and mix type
- Contractors obtained mix samples from two or three full lots from each shadow project
- NCAT conducted HWTT, IDEAL-CT, etc. on samples
  - Summary of within-lot variability for BMD test results



| IDEAL CT |        |         |          |       |
|----------|--------|---------|----------|-------|
| Project  | Lot    | Average | Std. Dev | COV   |
| 1        | 1      | 47.0    | 7.4      | 15.6% |
|          | 2      | 48.0    | 4.0      | 8.4%  |
| 2        | 2      | 58.2    | 9.1      | 15.7% |
|          | 3      | 62.8    | 19.6     | 31.1% |
| 3        | 2      | 62.7    | 6.4      | 10.2% |
|          | 3      | 69.7    | 27.7     | 39.7% |
| 4        | 4      | 73.3    | 17.8     | 24.3% |
|          | 2      | 86.2    | 7.6      | 8.8%  |
| 5        | 3      | 83.8    | 10.7     | 12.8% |
|          | 4      | 89.0    | 6.0      | 6.7%  |
| 6        | 4      | 40.1    | 4.3      | 10.7% |
|          | 5      | 44.3    | 8.8      | 19.9% |
| 7        | 6      | 51.3    | 5.2      | 10.1% |
|          | 9 & 11 | 46.2    | 3.6      | 7.8%  |
| 8        | 10     | 51.2    | 7.7      | 15.1% |
|          | 3 & 6  | 106.7   | 16.8     | 15.7% |
| 9        | 4      | 113.5   | 7.8      | 6.9%  |
|          | 5      | 120.4   | 8.9      | 7.4%  |
| 10       | 3      | 45.1    | 2.0      | 4.4%  |
|          | 4      | 51.0    | 4.6      | 9.1%  |
| 1        | 5      | 43.4    | 0.6      | 1.3%  |
|          | 8      | 51.5    | 8.9      | 17.2% |
| 2        | 9      | 58.9    | 5.2      | 8.8%  |
|          | 10     | 57.5    | 5.5      | 9.5%  |

Minimum COV: 1.3%  
Mean COV: 13.1%  
Maximum COV: 39.7%

| HWTT - Corrected Rut Depth 20,000 passes |        |         |          |       |
|--|--------|---------|----------|-------|
| Project                                  | Lot    | Average | Std. Dev | COV   |
| 1  | 1      | 10.7    | 2.2      | 20.4% |
|  | 2      | 11.0    | 1.4      | 13.1% |
| 2  | 2      | 16.4    | 2.8      | 16.8% |
|  | 3      | 16.2    | 0.7      | 4.4%  |
| 3  | 2      | 9.0     | 0.4      | 4.1%  |
|  | 3      | 11.0    | 0.4      | 4.1%  |
| 4  | 4      | 10.6    | 1.2      | 11.7% |
|  | 2      | 15.9    | 1.6      | 10.3% |
| 5  | 3      | 16.2    | 1.3      | 8.0%  |
|  | 4      | 17.3    | 3.0      | 17.6% |
| 6  | 4      | 10.5    | 1.0      | 9.9%  |
|  | 5      | 11.2    | 0.7      | 5.8%  |
| 7  | 6      | 10.5    | 0.7      | 7.0%  |
|  | 9 & 11 | 11.3    | 1.0      | 8.7%  |
| 8  | 10     | 11.6    | 1.6      | 13.5% |
|  | 3 & 6  | 11.7    | 0.7      | 5.6%  |
| 9  | 4      | 13.1    | 3.4      | 26.4% |
|  | 5      | 16.4    | 3.3      | 20.1% |
| 10                                       | 3      | 10.2    | 1.2      | 11.9% |
|  | 4      | 10.2    | 1.0      | 10.0% |
| 1  | 5      | 8.4     | 1.2      | 14.3% |
|  | 8      | 9.7     | 0.9      | 9.3%  |
| 2  | 9      | 11.0    | 1.1      | 9.6%  |
|  | 10     | 10.6    | 1.1      | 10.6% |

Minimum COV: 4.1%  
Mean COV: 10.9%  
Maximum COV: 26.4%

| SN      |          |                          |                            |       |
|---------|----------|--------------------------|----------------------------|-------|
| Project | Lot      | Average LC <sub>SN</sub> | Std. Dev. LC <sub>SN</sub> | COV   |
| 1       | Lot 1    | 4342                     | 1868                       | 43.0% |
|         | Lot 2    | 3644                     | 1135                       | 31.1% |
| 2       | Lot 2    | 4232                     | 1692                       | 40.0% |
|         | Lot 3    | 3188                     | 1356                       | 42.5% |
| 3       | Lot 2    | 6011                     | 3483                       | 57.9% |
|         | Lot 3    | 4348                     | 935                        | 21.5% |
| 4       | Lot 4    | 4424                     | 1002                       | 22.6% |
|         | Lot 2    | 3101                     | 797                        | 25.7% |
| 5       | Lot 3    | 4502                     | 1898                       | 42.2% |
|         | Lot 4    | 3089                     | 1638                       | 53.0% |
| 6       | Lot 4    | 7997                     | 2723                       | 34.1% |
|         | Lot 5    | 5743                     | 3587                       | 62.5% |
| 7       | Lot 6    | 5828                     | 2706                       | 46.4% |
|         | Lot 9&11 | 3289                     | 487                        | 14.8% |
| 8       | Lot 10   | 4045                     | 1819                       | 45.0% |
|         | Lot 3&6  | 2530                     | 440                        | 17.4% |
| 9       | Lot 4    | 2426                     | 590                        | 24.3% |
|         | Lot 5    | 2476                     | 203                        | 8.2%  |
| 10      | Lot 3    | 2995                     | 951                        | 31.8% |
|         | Lot 4    | 3138                     | 1205                       | 38.4% |
| 1       | Lot 5    | 3150                     | 770                        | 24.4% |
|         | Lot 8    | 3955                     | 1149                       | 29.1% |
| 2       | Lot 9    | 3460                     | 860                        | 24.9% |
|         | Lot 10   | 3500                     | 1149                       | 32.8% |

Minimum COV: 8.2%  
Mean COV: 33.5%  
Maximum COV: 62.5%

- Contractors provided asphalt and air void contents
  - Summary of within-lot variability

| Asphalt Content |     |           |           |      |
|-----------------|-----|-----------|-----------|------|
| Project         | Lot | Average e | Std. Dev. | COV  |
| 1               | 1   | 6.1       | 0.2       | 2.6% |
|                 | 2   | 6.3       | 0.2       | 3.8% |
| 2               | 2   | 5.6       | 0.1       | 1.3% |
|                 | 3   | 5.5       | 0.1       | 1.8% |

Minimum COV: 1.3%  
Mean COV: 2.8%  
Maximum COV: 7.2%

| Air Voids |     |           |           |       |
|-----------|-----|-----------|-----------|-------|
| Project   | Lot | Average e | Std. Dev. | COV   |
| 1         | 1   | 3.3       | 0.4       | 12.8% |
|           | 2   | 3.1       | 0.3       | 10.2% |
| 2         | 2   | 2.8       | 0.1       | 4.1%  |
|           | 3   | 2.8       | 0.1       | 3.6%  |

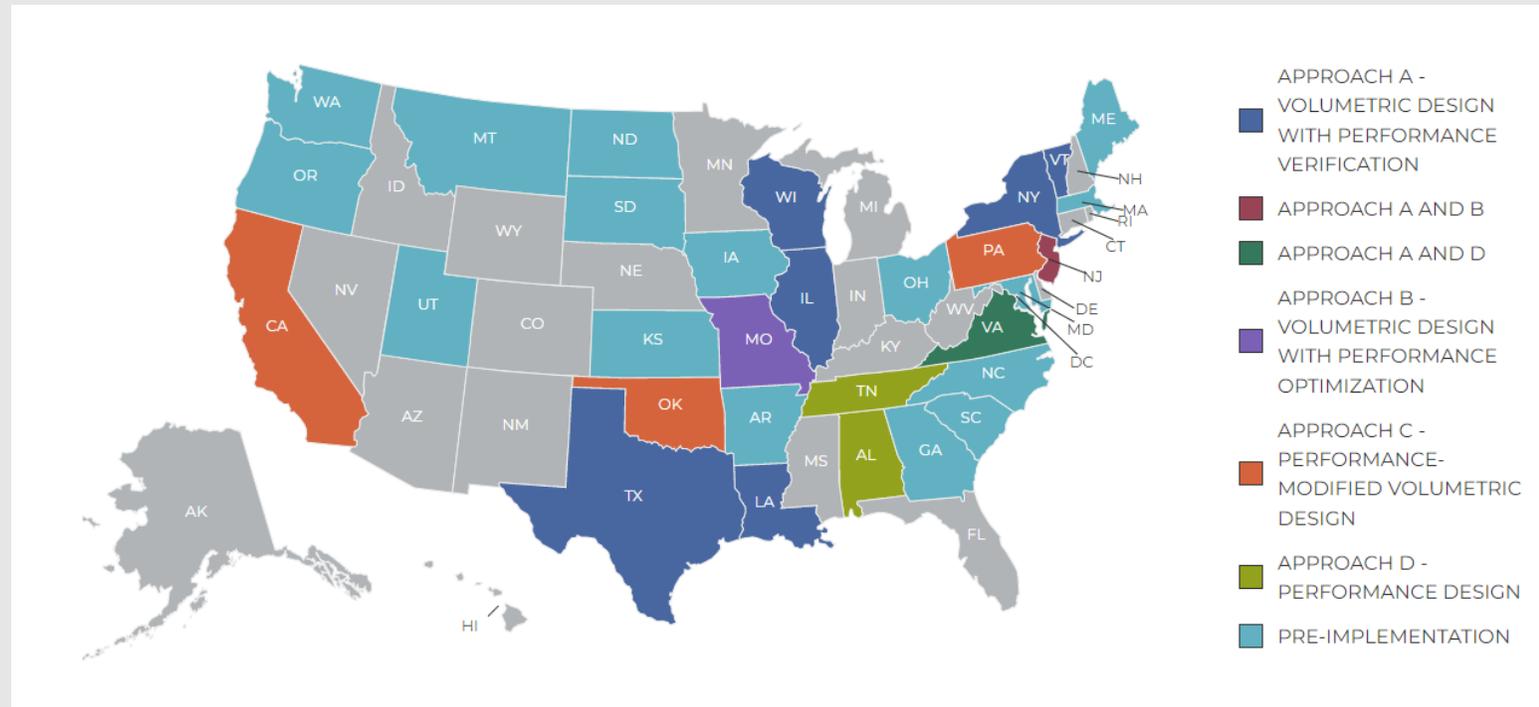
Minimum COV: 1.7%  
Mean COV: 10.4%  
Maximum COV: 21.3%



# BMD Pilot Projects in WI

- How do we compare with others?
  - In 2020, WisDOT developed an SPV for BMD pilot projects selected from percent within limits (PWL) projects
    - One pilot project per region
    - Mix design stage, not production
    - HWTT and IDEAL-CT

## Implementation Efforts

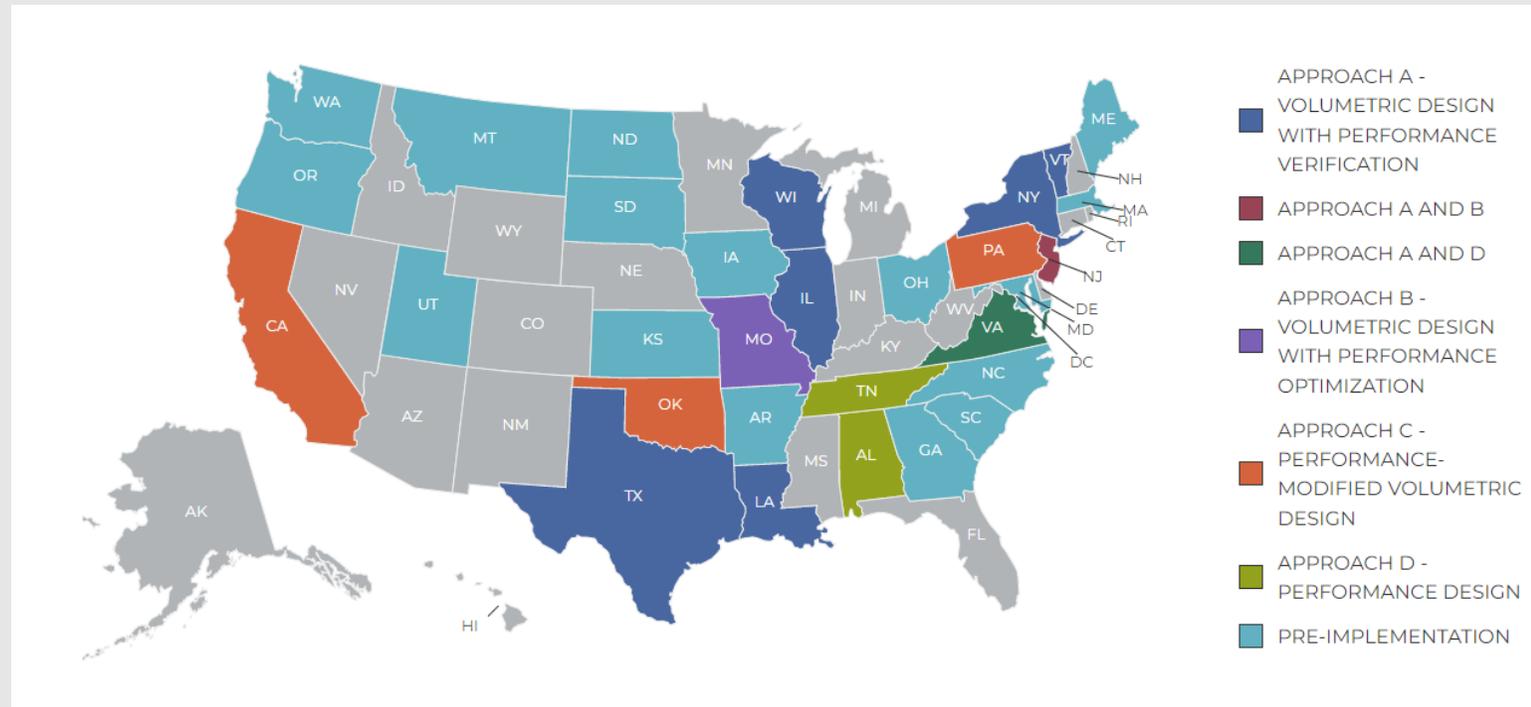


<https://www.asphaltpavement.org/expertise/engineering/resources/bmd-resource-guide/implementation-efforts>

# BMD Pilot Projects in WI

- How do we compare with others?
  - WisDOT developed an SPV for BMD pilot projects selected from PWL projects
    - From 2021-2023: the criteria set for HWT test were based on **No. of passes to failure** and **SIP**
    - From 2023-present: the criterial set for HWT have been based on **CRD** and **SN**

## Implementation Efforts



<https://www.asphaltpavement.org/expertise/engineering/resources/bmd-resource-guide/implementation-efforts>

\*Note: SIP is the abbreviation of stripping inflection point.

# BMD Pilot Projects in WI

- SPV used for pilot BMD projects since 2020

## HMA Pavement Balanced Mix Design

### A Description

Conform to standard specification 450 and 460 except as modified in this special provision.

This special provision incorporates balanced mix design (BMD) into the mix design procedures specified in standard specification 460. This specification applies to the primary upper layer mixture under the following bid item: Enter Bid Item #. Mix designs will be tested by the Hamburg Wheel-Track Test (HWT) according to AASHTO T 324 as modified by CMM [836.6.10.1](#) and the Indirect Tensile Cracking Test at Intermediate Temperature (CT-Index) according to ASTM D8225 as modified by CMM [836.6.10.2](#).

- BMD is incorporated at the mix design stage for certain PWL projects
- Applies to upper layer mixtures
- Mix designs are tested using HWTT and IDEAL-CT methods



# BMD Pilot Projects in WI

- SPV used for pilot BMD projects since 2020
  - Mix design testing criteria from 2021 to 2023

| Binder Designation Level <sup>[1]</sup>   | S               | H               | V               | E               |
|---|-----------------|-----------------|-----------------|-----------------|
| Hamburg Wheel Tracking<br>(AASHTO T 324 as modified in CMM 836.6.10.1)<br>Passes to 12.5 mm rut depth<br>Stripping Inflection Point | 10,000<br>8,000 | 10,000<br>8,000 | 20,000<br>8,000 | 20,000<br>8,000 |
| IDEAL-CT <sup>[2]</sup><br>(ASTM D8225 as modified in CMM 836.6.10.2)<br>CT-Index   | 30              | 30              | 30              | 30              |

→ To ensure rutting and moisture damage resistance

→ To ensure cracking resistance

- Mix design testing criteria from 2023 to present

| Mixture Type   | LT                | MT               | HT               | SMA              |
|--|-------------------|------------------|------------------|------------------|
| Hamburg Wheel Tracking<br>(WTM T324)<br>Corrected Rut Depth @ 20,000 Passes (mm)<br>Stripping Number (LC <sub>SN</sub> ) | ≤ 12.0<br>≥ 3,000 | ≤ 7.5<br>≥ 3,000 | ≤ 5.0<br>≥ 3,000 | ≤ 4.0<br>≥ 3,000 |
| IDEAL-CT<br>(ASTM D8225 as modified in CMM 836.6.10.2)<br>CT-Index   | ≥ 30              | ≥ 30             | ≥ 30             | ≥ 80             |

→ To ensure rutting and moisture damage resistance

→ To ensure cracking resistance

- Testing during the production was for information purpose only



# BMD Shadow Projects in WI

- Loose mixture were procured from:
  - PWL projects from 2020 to 2023
  - Certain PWL and non-PWL projects since 2023
- BMD performance tests
  - IDEAL-CT
  - HWTT
- Participants
  - Department (Central Office)
  - Contractors
- Results from 287 mixtures have been analyzed so far

# BMD Shadow Projects in WI

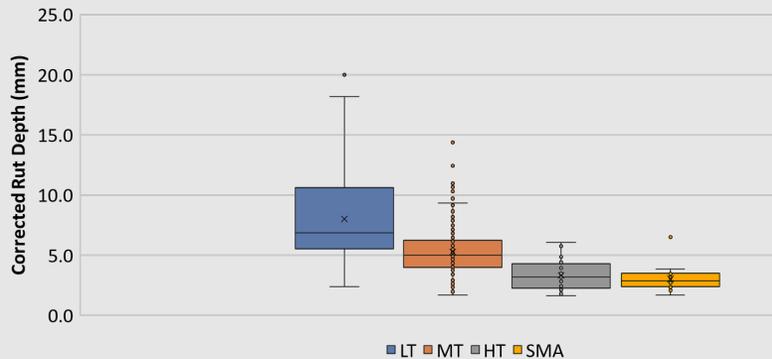
- HWTT was conducted @ 46°C on
  - Short-term aged (reheated) mixtures
- IDEAL-CT was conducted @ 25°C on
  - Both reheated and long-term aged mixtures
- No. of specimens fabricated per mixture
  - Reheated (@ 135°C for 2 hours)
    - HWTT: 4 specimens
    - IDEAL-CT: 4 specimens
  - Long-term aged (@ 135°C for 6 hours)
    - IDEAL-CT: 4 specimens
  - Total number of specimens tested by 2023:  $287 \times 3 \times 4 = 3,444$

# BMD Shadow Projects in WI

- The influence of traffic level and/or aggregate skeleton on BMD test results

## Corrected Rut Depth (CRD)

HWT CRD @ 20,000 Passes Distribution by Mixture Traffic Level



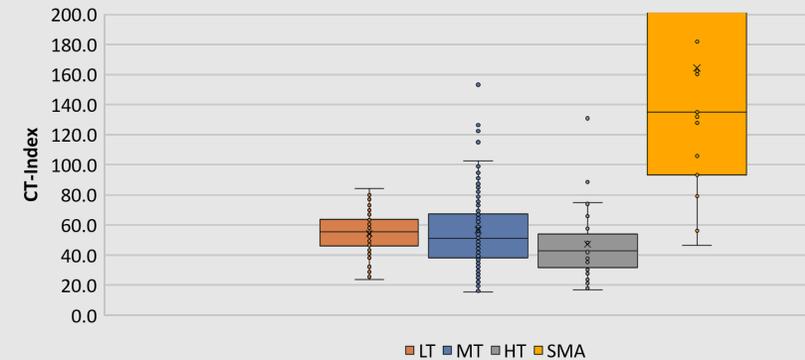
## Stripping Number (SN)

HWT LCSN Distribution by Mixture Traffic Level



## CT-Index

IDEAL-CT LTA6 Distribution by Mixture Traffic Level



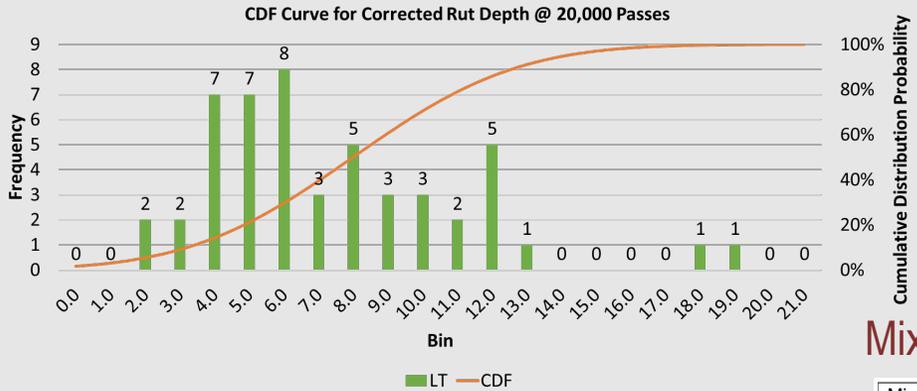
## Mix design testing criteria from 2023 to present

| Mixture Type  | LT      | MT      | HT      | SMA     |
|---|---------|---------|---------|---------|
| Hamburg Wheel Tracking (WTM T324)                   |         |         |         |         |
| Corrected Rut Depth @ 20,000 Passes (mm)            | < 12.0  | < 7.5   | < 5.0   | < 4.0   |
| Stripping Number (LC <sub>SN</sub> )                | ≥ 3,000 | ≥ 3,000 | ≥ 3,000 | ≥ 3,000 |
| IDEAL-CT (ASTM D8225 as modified in CMM 836.6.10.2) |         |         |         |         |
| CT-Index  | ≥ 30    | ≥ 30    | ≥ 30    | ≥ 80    |

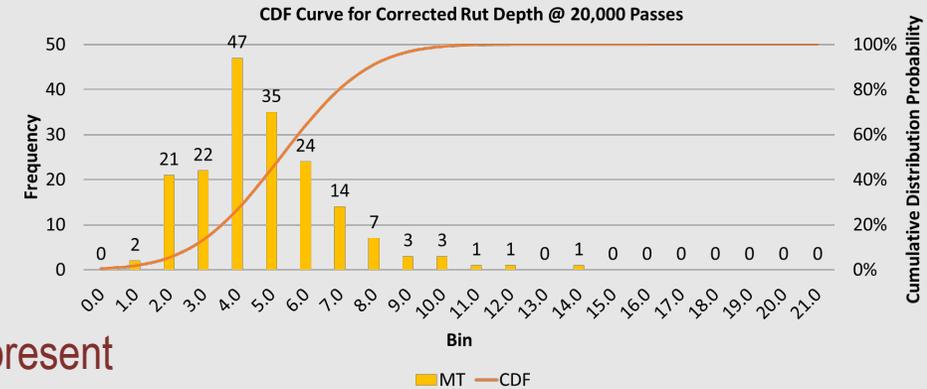
# BMD Shadow Projects in WI

- CRD cumulative distribution function (CDF) curves

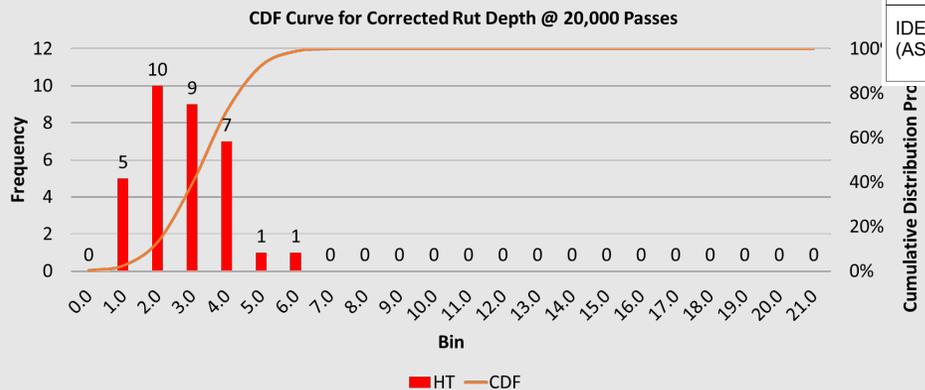
LT



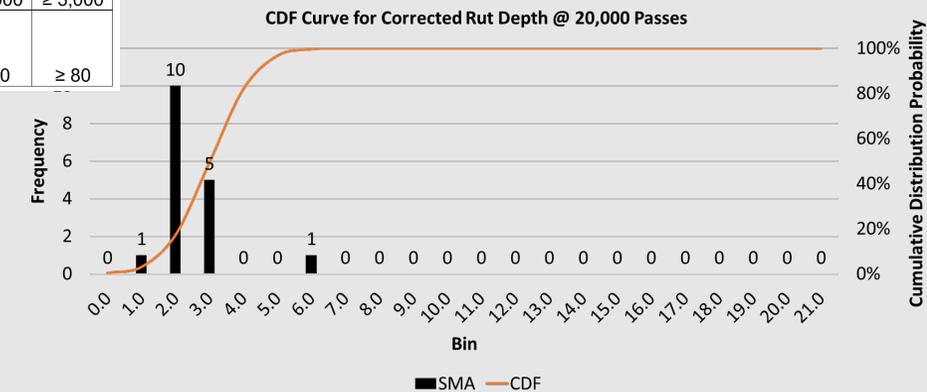
MT



HT



SMA



## Mix design testing criteria from 2023 to present

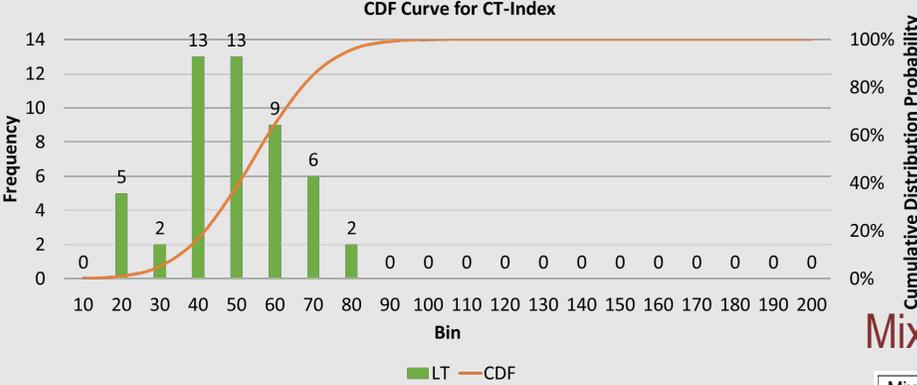
| Mixture Type  | LT      | MT      | HT      | SMA     |
|---|---------|---------|---------|---------|
| Hamburg Wheel Tracking (WTM T324)                   |         |         |         |         |
| Corrected Rut Depth @ 20,000 Passes (mm)            | ≤ 12.0  | ≤ 7.5   | ≤ 5.0   | ≤ 4.0   |
| Stripping Number (LC <sub>SN</sub> )                | ≥ 3,000 | ≥ 3,000 | ≥ 3,000 | ≥ 3,000 |
| IDEAL-CT (ASTM D8225 as modified in CMM 836.6.10.2) |         |         |         |         |
| CT-Index  | ≥ 30    | ≥ 30    | ≥ 30    | ≥ 80    |



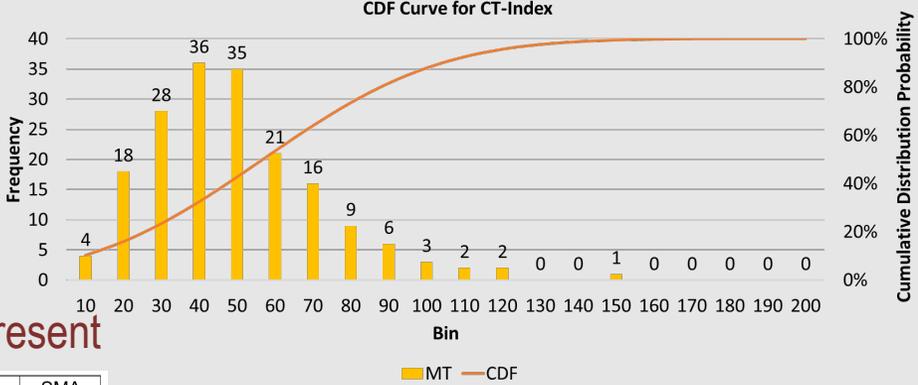
# BMD Shadow Projects in WI

- CT-Index cumulative distribution function (CDF) curves

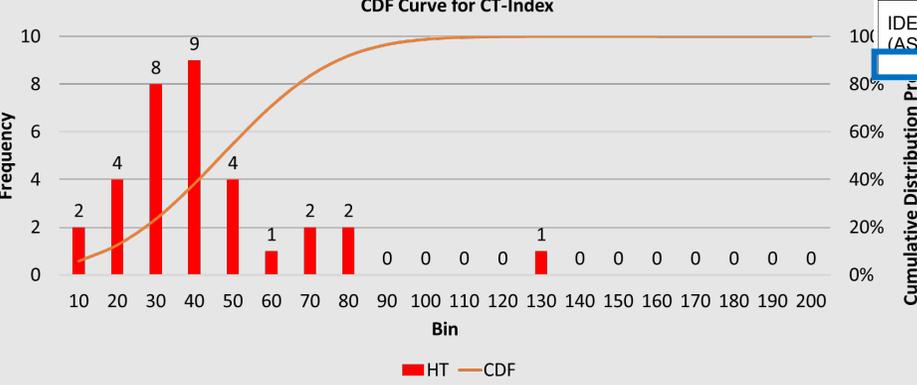
LT



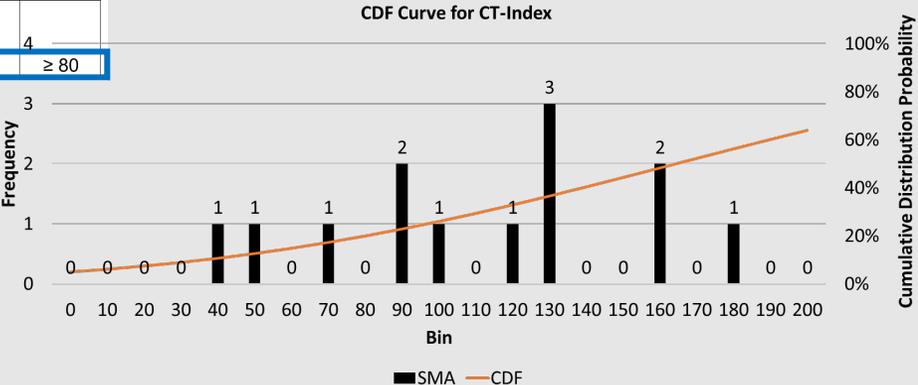
MT



HT

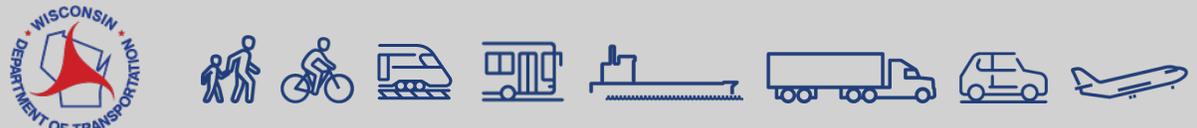


SMA



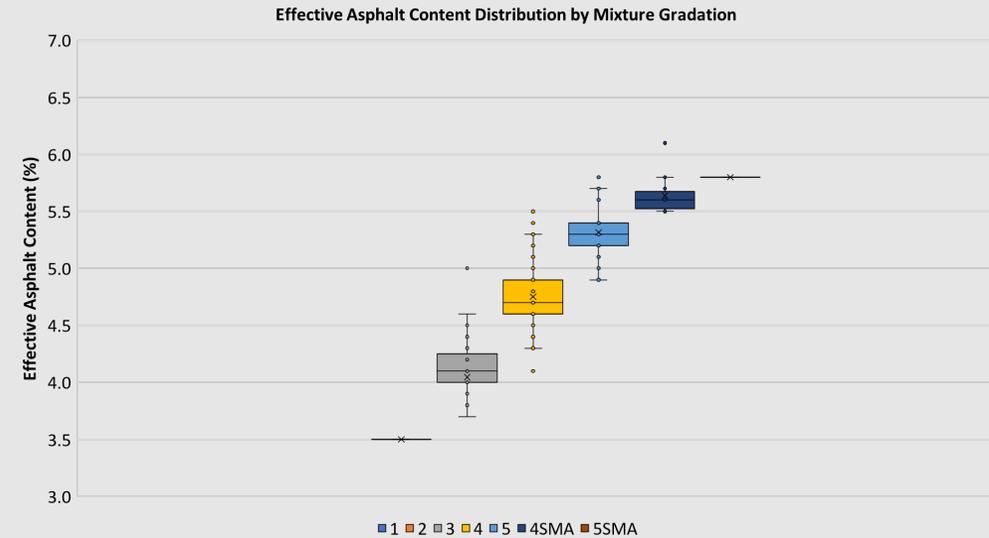
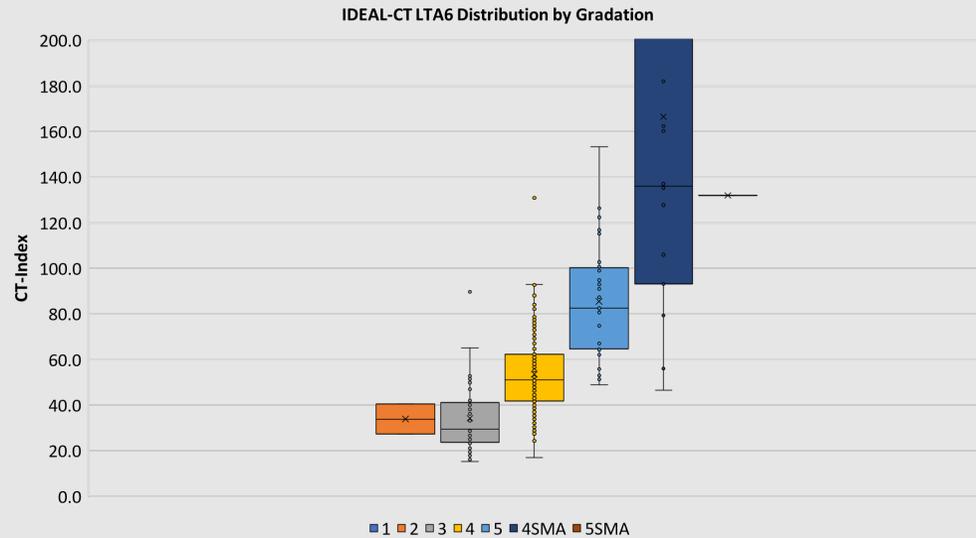
Mix design testing criteria from 2023 to present

| Mixture Type  | LT      | MT      | HT      | SMA     |
|---|---------|---------|---------|---------|
| Hamburg Wheel Tracking (WTM T324)                   |         |         |         |         |
| Corrected Rut Depth @ 20,000 Passes (mm)            | ≤ 12.0  | ≤ 7.5   | ≤ 5.0   | ≤ 4.0   |
| Stripping Number (LC <sub>SN</sub> )                | ≥ 3,000 | ≥ 3,000 | ≥ 3,000 | ≥ 3,000 |
| IDEAL-CT (ASTM D8225 as modified in CMM 836.6.10.2) |         |         |         | 4       |
| CT-Index  | ≥ 30    | ≥ 30    | ≥ 30    | ≥ 80    |



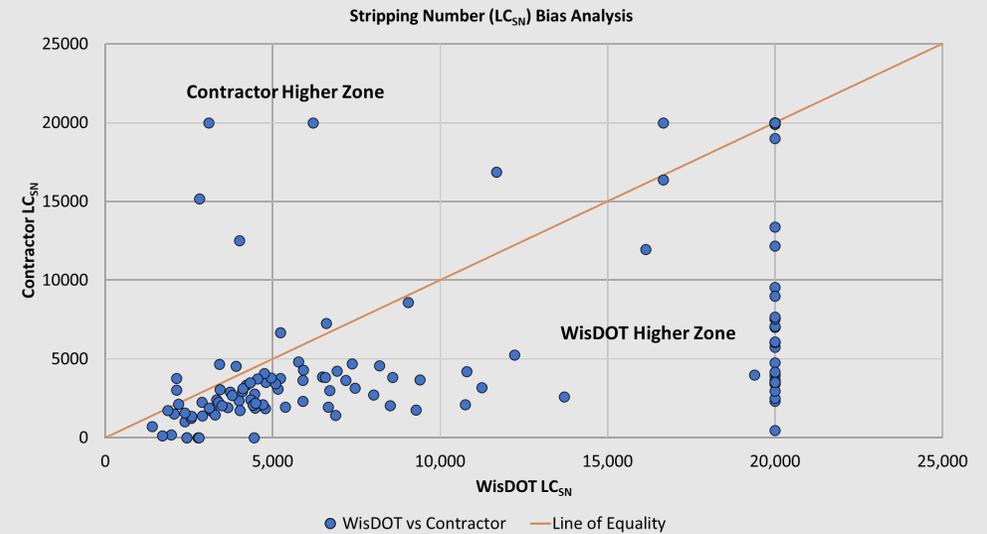
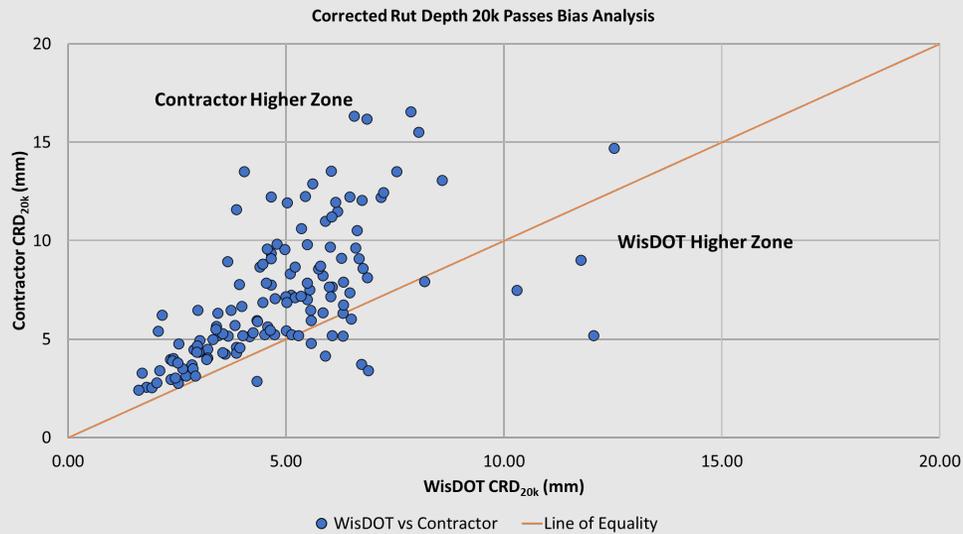
# BMD Shadow Projects in WI

- The influence of aggregate size on cracking resistance performance



# BMD Shadow Projects in WI

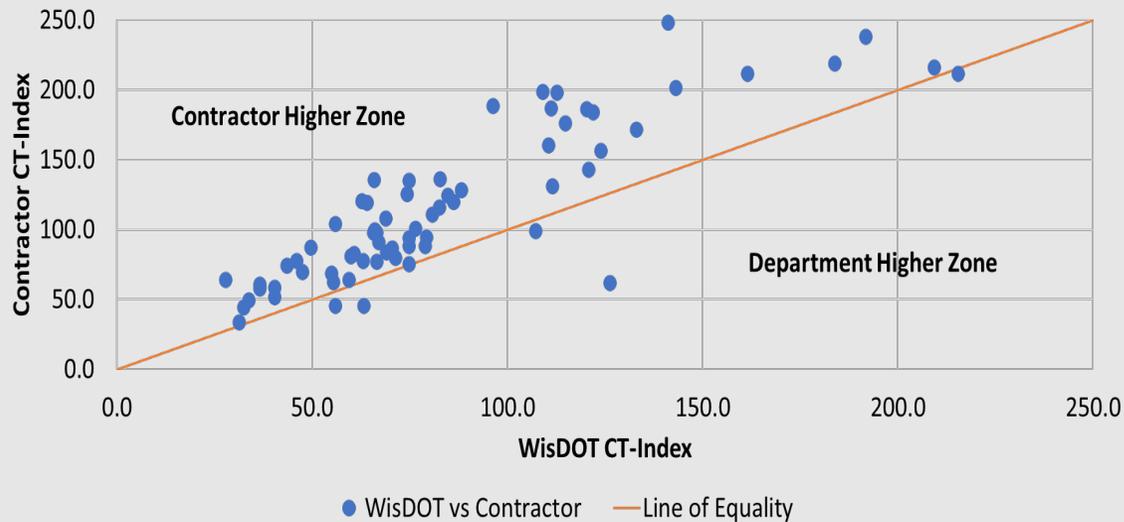
- Bias analysis
  - CRD and SN data



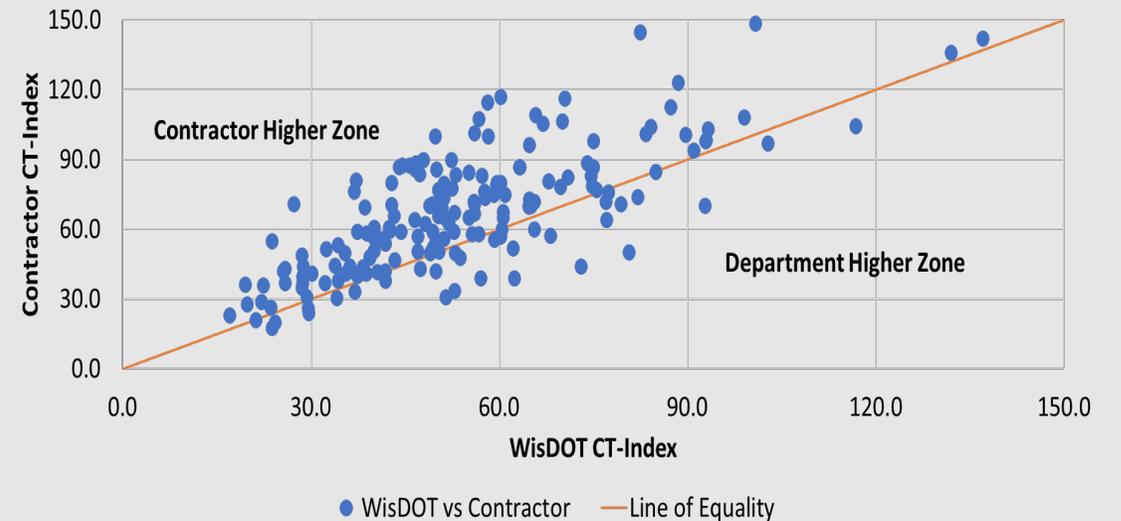
# BMD Shadow Projects in WI

- Bias analysis
  - CT-Index data

IDEAL-CT: Plant Aged Bias Analysis



IDEAL-CT: LTA6 Bias Analysis



# BMD Shadow Projects in WI

- What does bias analysis data tell us?
  - Results from IDEAL-CT and HWTT indicated that on average, among the 287 mixtures tested, contractor test results exhibited less aging than those from the department
  - Based on these determinations, sample handling, preparation, and testing procedures were scrutinized, and a detailed formal procedure was issued for future performance testing

# BMD Shadow Projects in WI

- What was done to decrease the interlaboratory variability?
  - We thought about every single possible scenario ....

## BMD Sample Preparation

This aging / conditioning and handling procedure was developed by the WisDOT Bureau of Technical Services HMA Unit to minimize the aging and conditioning influences on the balanced mix design test results.

### 1. Reheating:

- Place one box each of IDEAL-CT Plant Aged (PA), IDEAL-CT Long-Term Aged (LTA6), and Hamburg Wheel Test (HWT), unopened, in a preheated oven at  $135^{\circ}\text{C} \pm 3^{\circ}\text{C}$  ( $275^{\circ}\text{F} \pm 5^{\circ}\text{F}$ ) for 2 hours  $\pm$  5 minutes. Boxes should remain shut for the duration of the reheating procedure.

### 2. Splitting:

#### A. Immediately after reheating:

- Split five, approximately 2,600g\*, specimens from the first box: one for a trial puck, and four for IDEAL-CT (PA) pucks. Place the split specimens into small bowls or pans.
- Split four, approximately 2,600g\*, specimens from the second box for the HWT pucks. Place the split specimens into small bowls or pans.
- Split four, approximately 2,600g\*, specimens from the third box for IDEAL-CT (LTA6). Place the specimens in shallow pans (approximately 13" x 9" x 2"). The mix should be  $\frac{3}{4}$ " - 1" deep in the pan. Cover the pans with foil and store at room temperature ( $23 - 25.5^{\circ}\text{C} / 73 - 78^{\circ}\text{F}$ ) to prepare for long-term aging the following day.

- Continue to compaction of the trial puck in step 3 below and begin to cool the IDEAL-CT (PA) and HWT specimens to room temperature ( $23 - 25.5^{\circ}\text{C} / 73 - 78^{\circ}\text{F}$ ) for 2 hours  $\pm$  5 minutes in front of a fan.

\*NOTE: The weight of the split specimens will be approximately 2,600 grams to produce pucks that are 61 mm tall at an air void content of  $7.0\% \pm 0.5\%$ . The Gmm 4-point running average corresponding to the mix can be used to estimate the split specimen weights at 7.0% air voids.

### 3. Compaction: Trial, Plant Aged and HWT Pucks

- Compact the trial specimen to a height of 61 mm and  $7.0\% \pm 0.5\%$  air voids at  $127^{\circ}\text{C} \pm 3^{\circ}\text{C}$  ( $261^{\circ}\text{F} \pm 5^{\circ}\text{F}$ ). Record the length of time (T) required to compact the specimen to the required height.
- Measure the Gmb after the sample has cooled for at least 1 hour in front of a fan. Determine split specimen weight adjustment (W), if needed, to meet the air void target ( $7.0\% \pm 0.5\%$ ) for the remaining samples to be compacted.
- Adjust all specimen batch weights (including the LTA6 specimens) according to the weight adjustment (W) determined in step 3B.
- Reheat the IDEAL-CT (PA) and HWT specimens in a preheated oven at  $135^{\circ}\text{C} \pm 3^{\circ}\text{C}$  ( $275^{\circ}\text{F} \pm 5^{\circ}\text{F}$ ) for 2 hours  $\pm$  5 minutes. Place the specimens in the oven, one specimen at a time; space their placement times by the length of time (T) determined in step 3A. This is to ensure that each specimen is aged the same amount of time while others are being compacted.
- Compact remaining specimens at the determined adjusted weights to a height of 61 mm and  $7.0\% \pm 0.5\%$  air voids at  $135^{\circ}\text{C} \pm 3^{\circ}\text{C}$  ( $275^{\circ}\text{F} \pm 5^{\circ}\text{F}$ ).

- Measure the Gmb after the specimens have cooled for at least 1 hour in front of a fan. Verify the target air void content ( $7.0\% \pm 0.5\%$ ) was achieved for all specimens.

### 4. Compaction: Long-Term Aged Pucks

- Uncovered pans are placed in a preheated oven for 6 h  $\pm$  5 min at a temperature of  $135 \pm 3^{\circ}\text{C}$  ( $275 \pm 5^{\circ}\text{F}$ ). Place the specimens in the oven, one specimen at a time; space their placement times by the length of time (T) determined in step 3A. This is to ensure that each specimen is aged the same amount of time while others are being compacted.
- After the 6-hour aging, compact specimens at the determined adjusted weights to a height of 61 mm and  $7.0\% \pm 0.5\%$  air voids at  $135^{\circ}\text{C} \pm 3^{\circ}\text{C}$  ( $275^{\circ}\text{F} \pm 5^{\circ}\text{F}$ ).
- Measure the Gmb after the sample has cooled for at least 1 hour in front of a fan. Verify that target air void content ( $7.0\% \pm 0.5\%$ ) was achieved for all specimens.

### 5. Testing

- Hamburg Wheel Test (AASHTO T324 as modified below)
  - Test temperature is  $46^{\circ}\text{C} \pm 1^{\circ}\text{C}$  ( $115^{\circ}\text{F} \pm 2^{\circ}\text{F}$ ).
  - Test until 20,000 passes or 12.5-mm rut depth.
- IDEAL-CT (ASTM D8225 as modified below)
  - Condition samples in water bath at  $25^{\circ}\text{C} \pm 1^{\circ}\text{C}$  for 2 hours  $\pm$  10 minutes.

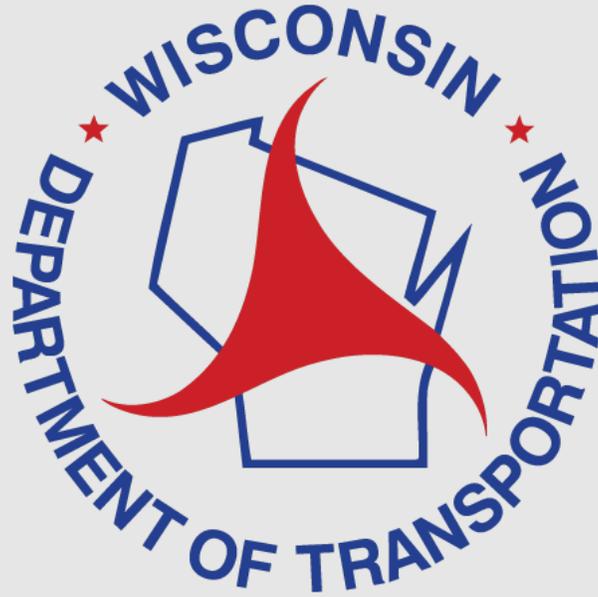
# BMD Shadow Projects in WI

- Round Robin Study results

$$Z = \frac{x_i - \bar{x}}{\sigma_s}$$

$$d2s = 2\sigma_s\sqrt{2}$$

|            | Lab                   | IDEAL-CT     |       | Hamburg Wheel Test |                   |        |         |         |          |        |
|------------|-----------------------|--------------|-------|--------------------|-------------------|--------|---------|---------|----------|--------|
|            |                       | Planted Aged | LTA-6 | Rut Depth          | Passes to Failure | SIP    | CRD 10k | CRD 20k | LCSN     | LCST   |
|            | Lab 1                 | 92.5         | 69.8  | 9.21               | 20,000            | 14,401 | 4.15    | 5.12    | 6,952    | 23,743 |
|            | Lab 2                 | 91.2         | 60.9  | 5.71               | 20,000            | #N/A   | 4.11    | 5.39    | 20,000   | #N/A   |
|            | Lab 3                 | 109.7        | 87.1  | 8.20               | 20,000            | #N/A   | 5.13    | 6.67    | 17,000   | #N/A   |
|            | Lab 4                 | 72.8         | 67.8  | 5.52               | 20,000            | #N/A   | 4.46    | 5.46    | 20,000   | #N/A   |
| Statistics | <b>Average:</b>       | 91.6         | 71.4  | 7.2                | 20,000.0          | #N/A   | 4.5     | 5.7     | 15,988.0 | #N/A   |
|            | <b>Median:</b>        | 91.9         | 68.8  | 7.0                | 20,000.0          | #N/A   | 4.3     | 5.4     | 18,500.0 | #N/A   |
|            | <b>Samp Std. Dev:</b> | 15.08        | 11.14 | 1.83               | 0.00              | #N/A   | 0.47    | 0.69    | 6187.78  | #N/A   |
|            | <b>COV:</b>           | 16.5%        | 15.6% | 25.6%              | 0.0%              | #N/A   | 10.6%   | 12.2%   | 38.7%    | #N/A   |
| Z-Scores   | <b>Z-Score Lab 1:</b> | 0.06         | -0.14 | 1.12               | #N/A              | #N/A   | -0.66   | -0.78   | -1.46    | #N/A   |
|            | <b>Z-Score Lab 2:</b> | -0.02        | -0.94 | -0.79              | #N/A              | #N/A   | -0.75   | -0.39   | 0.65     | #N/A   |
|            | <b>Z-Score Lab 3:</b> | 1.20         | 1.41  | 0.57               | #N/A              | #N/A   | 1.42    | 1.47    | 0.16     | #N/A   |
|            | <b>Z-Score Lab 4:</b> | -1.24        | -0.32 | -0.89              | #N/A              | #N/A   | -0.01   | -0.29   | 0.65     | #N/A   |
| Quartiles  | <b>IQR:</b>           | 10.2         | 8.1   | 2.8                | 0                 | #N/A   | 0.49    | 0.44    | 5,512.0  | #N/A   |
|            | <b>Q1:</b>            | 86.6         | 66.1  | 5.7                | 20,000            | #N/A   | 4.14    | 5.32    | 14,488.0 | #N/A   |
|            | <b>Q3:</b>            | 96.8         | 74.1  | 8.5                | 20,000            | #N/A   | 4.63    | 5.76    | 20,000.0 | #N/A   |
|            | <b>Low Range:</b>     | 71.3         | 54.0  | 1.5                | 20,000            | #N/A   | 3.41    | 4.66    | 6220     | #N/A   |
|            | <b>High Range:</b>    | 112.1        | 86.2  | 12.6               | 20,000            | #N/A   | 5.36    | 6.42    | 28268    | #N/A   |
|            | <b>d2s:</b>           | 42.6         | 31.5  | 5.2                | 0.0               | #N/A   | 1.3     | 1.9     | 17,501.7 | #N/A   |



Any questions or comments?

**Thank You!**